

SEA FISH INDUSTRY AUTHORITY  
Industrial Development Unit

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REPORT OF THE SEA FISH INDUSTRY AUTHORITY  
TOWING REQUIREMENTS FOR A DEMERSAL PAIR TRAWL  
(2 x 340 H.P. VESSELS)

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Technical Report No. 256  
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C. Brady  
January 1985

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Industrial Development Unit

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TOWING REQUIREMENTS FOR A DEMERSAL PAIR TRAWL  
(2 x 340 H.P. VESSELS)

SUMMARY

This report contains the performance data of a F.M.A. Buckie Pair Trawl - BT154 rigged with two bridles and Rockhopper gear.

The net was towed between two vessels - the Aquila and the Poseidon - each having nominally 365 H.P. installed. The vessels were instrumented to record the performance parameters and will be the subject of further investigations to be covered in a later report.

The trials were carried out in March 1984 jointly by the SFIA and DAFS who instrumented the trawl. It is from DAFS recorded measurements of the net that this report has been compiled.

The report expresses the power requirements in terms of warp tensions and settings of net speed, warp length and vessel distance. While it would have been of greater convenience to fishermen to use horsepower or fuel flow rather than warp tension as an indicator of vessel performance, an assumed pull/power characteristic would not be valid for other vessels. The two vessels used in the trials had dissimilar characteristics; the reasons for this are being investigated and will be discussed in a later report. The requirement for any net setting are defined and the data is presented in a manner which can readily be used by skippers provided that their vessels are equipped with warp tension meters.

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Contents

	Page No.
<b>SUMMARY</b>	
1 <b>INTRODUCTION</b>	1
2 <b>TRAWL DESCRIPTION</b>	3
3 <b>VESSEL DESCRIPTIONS</b>	4
3.1    Aquila	4
3.2    Poseidon	5
4 <b>TRIALS LOG</b>	6
5 <b>PROCEDURE</b>	8
6 <b>RESULTS AND DATA ANALYSIS</b>	9
6.1    Derived Formula	9
6.1.1 Single Warp Tension	9
6.1.2 Horizontal Opening	9
6.1.3 Vertical Opening	10
6.2    Comparison of Predicted and Recorded Values	10
7 <b>RESULTS</b>	11

Contents Contd.

		Page No.
8	<b>DICUSSIONS</b>	16
	8.1 General	16
	8.2 Horizontal Opening	18
	8.3 Vertical Opening	18
9	<b>CONCLUSIONS</b>	20
	9.1 Horizontal Opening	20
	9.2 Vertical Opening	20
	9.3 Vessel Speed	20
	9.4 Warp	21
	9.5 Vessel Distance	21
	9.6 Water Depth	21

**FIGURES:**

1 - 4	Single Warp Tension vers Net Speed
5 - 8	Horizontal Opening vers Net Speed
9 - 11	Vertical Opening vers Net Speed
12 - 14	Comparison of Recorded and Predicted Values
15 - 18	Prediction of Single Warp Tension
19 - 22	Prediction of Horizontal Opening
23 - 26	Prediction of Vertical Opening

**TABLES:**

1 - 3	Analysed Values for Average Tow Parameters on Trial
4 - 12	Predicted Values for Constant Water Depths
13	Effect of Changing One Variable

**APPENDICES:**

I	FMA Buckie Pair Trawl BT154 (with 2 Bridles and Rockhopper Gear)
II	Details of 3 Bridle Arrangement and Traditional Bobbin Rig for BT154 Trawl
III	Average Results of Recorded Parameters Derived by DAFS
IV	Summary of Recorded Data Used in Analysis
V	Summary Presentation of Graphs for Predicting Warp Tension, Horizontal Opening and Vertical Opening

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1 **INTRODUCTION**

The trials described herein form part of the fuel conservation investigations commissioned by the Ministry of Agriculture, Fisheries and Food. (Commission A.1.3 JAB16).

The overall aim of the trials was to obtain information which may enable comparisons to be made of net efficiencies in terms of volume of water fished per unit work done and also to obtain data on vessel performance for correlation with prediction.

The trawl net is a F.M.A. Buckie Pair Trawl - BT154 rigged with two bridles and Rockhopper gear and was towed between two vessels - the Aquila and the Poseidon - each having nominally 365 installed horsepower. The trials were carried out during March 1984 in Broad Bay - Isle of Lewis - jointly by the SFIA and DAFS.

A measure of work done to tow the net may be expressed in terms of warp tension and in this manner is applicable regardless of the vessels towing it. The power requirements of the two vessels used in these trials and the relationships to the net and warp tensions will be the subject of a further report. This report therefore expresses the power requirements in terms of warp tensions and is addressed to defining the settings of speed, warp length and vessel distance, to give the best efficiency with respect to warp tension for any defined net opening. The data is presented in a manner which can readily be used by commercial vessels provided they are fitted with warp load meters. Data on actual powers recorded on the vessels has been analysed but is not presented here since the trials vessels had widely dissimilar power/pull characteristics and power or fuel consumption values would not necessarily be valid for other vessels.

The trials were carried out in conjunction with DAFS who instrumented the trawl. It is from their measurements that the data given in this report has been compiled. The engineering performance, geometry and drag of the various gear components will be reported by DAFS.

It is known that the angular arrangement of the warps has an effect on the efficiency of the gear because of their herding effect on the fish. This cannot be quantified by these trials and skippers must use their own experience to guide them. However the report does give an indication of the change in power demands and net opening when the settings of the warps are changed. Skippers may use this to assess whether the change in power and thus fuel is justified.

2            **TRAWL DESCRIPTION**

The trawl net chosen for the trials was F.M.A. Buckie Pair Trawl - BT154. This is a commercial two panel balloon trawl designed by the Buckie F.M.A. and a drawing is given in Appendix I.

As the design is confidential to FMA Buckie only the basic parameters are given.

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The net was primarily rigged with Rockhopper gear on a two bridle rig though measurements were also recorded with the net having a 3 bridle rig and also when rigged with conventional bobbins. These latter two rigs are diagrammatically detailed in Appendix II.

The technical details are as follows:

**Net**

Headline	37.5 metres	
	(1.55m+14.6m+5.2m+14.6m+1.55m) ..	(123 ft)
Footrope	45.8 metres	
	(0.6m+7.0m+30.5m+7.0m+0.6m) ..	(150 ft)
Hoppers	30.5 metres	..(100 ft)
Chain Leg	7.0 metres	..( 23 ft)
Adjust Chain	0.9 metres	..( 3 ft)
Floats	36 x 280 mm	..( 11 in)

**Bridles**

Upper	55.0 metres	..(180 ft)
Middle	27.5 metres	..( 90 ft)
Lower	55.0 metres	..(180 ft)

<b><u>Sweeps</u></b>	91.5 metres	..(300 ft)
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<b><u>Bobbins</u></b>	6.1 metres	..( 20 ft)
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3 VESSEL DESCRIPTIONS

The two vessels towing the net were the AQUILA - BCK 214, and the POSEIDON - BF 191. Both vessels are typical Scottish trawler seiners constructed in wood and fitted with three quarter length aluminium shelters. Outline technical specifications are as follows.

3.1 Aquila

Dimensions

Length Overall	... 16.76 m
Length Registered	15.24 m
Breadth	... 5.49 m
Depth	... 2.74 m

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Configuration

Conventional round bilge hull form with transom stern. Closed aluminium shelter extending from stem to aft side of wheelhouse. The main hull is subdivided into five compartments viz:

fore peak  
fishroom  
engine room  
crews cabin  
steering gear compartment

Machinery

Main Engine - Caterpillar D343 nominally rated at 365 HP @ 1800 RPM  
Gearbox - Caterpillar twin disc with 4.5:1 ratio  
Propeller - Brunton 'Superston 70' 4 bladed 52in dia 40in pitch right hand.

### 3.2 Poseidon

#### Dimensions

Length Overall	...	19.20 m
Length Registered	...	17.98 m
Breadth	...	6.50 m
Depth	...	3.76 m

#### Configuration

Conventional round bilge hull form with transom stern. Closed aluminium shelter extending from stem to aft side of wheelhouse. The main hull is subdivided into five compartments viz:

fore peak  
fishroom  
engine room  
crews cabin  
steering gear compartment

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#### Machinery

Main Engine - Caterpillar D343 nominally rated at 365 HP @ 1800 RPM  
Gearbox - Caterpillar twin disc with 4.5:1 ratio  
Propeller - Brunton manufacture 4 bladed 56in dia 37in pitch right hand.

4            TRIALS LOG

**27th February 1984**

Final instrumentation of vessels and net completed in Stornoway.

**28th February**

Preliminary tows carried out to test instrumentation. Tows terminated at 1500 hours due to worsening weather conditions.

**29th February**

Five tows carried out with part instrumentation prior to carrying out ten fully instrumented tows with 175 fathoms of warp out in a water depth of 12-26 fathoms.

**1st March 1984**

Five tows carried out with part instrumentation prior to carrying out ten full instrumented tows with 250 fathoms of warp out in a water depth of 45-56 fathoms.

**5th March**

Seven fully instrumented tows carried out with 350 fathom of warp out in a water depth of 47-58 fathoms. The gear became fast after the seventh tow and the trial was terminated for this warp length.

**6th March**

Ten fully instrumented tows carried out with 300 fathom of warp out in a water depth of 42-58 fathoms.

**7th March**

Six fully instrumented tows carried out with 300 fathom of warp out in a water depth of 46-55 fathoms and the net rigged with three bridles.

**8th March**

Nine fully instrumented tows carried out with 300 fathoms of warp out and five with 350 fathoms of warp out all using conventional bobbin gear. These tows were carried out in a water depth of 48-58 fathoms.

**9th March**

The trial now being complete the instrumentation was removed from the vessels.

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5            PROCEDURE

All tows, with the exception of those with 175 fathom of warp out, were made on the same tow between Triumpen Head and Tolsta Head across Broad Bay. Each tow consisted of up to 10 blocks (periods of 15 minutes whilst towing at constant RPM). Half the blocks were taken in one direction while the remainder were taken on the reciprocal course to allow tide corrections to be made.

Towing speeds and net speeds were measured using Braystoke logs. The warp tension at each of the vessels (position ref T1) was measured using strain gauge tension meters. Tensions were also recorded using self recording load cells, fitted at the following positions - (refer to Appendix I for diagram).

- T2 warp - sweep connection
- T3 mid sweeps
- T4 sweep - bridle connection
- T5 upper bridle-net
- T6 lower bridle-net

Self recording acoustic meters were fitted to measure wing end spread, mid bridle spread, fore sweep spread and headline height. A manometer was also used to measure headline height.

The average results of the various recorded parameters supplied by DAFS are given in Appendix III.

## 6 DATA ANALYSIS

The recorded parameter values read in this analysis are summarised in Appendix IV. The values have been analysed in such a manner that tidal effects have been accounted for and the data examined collectively to enhance the analysis.

### 6.1 Derived Formula

In the analysis methods using multiple linear regression have been used to determine formula which give the best fit to the recorded values and suitable graphical presentations to be derived for predicting the mouth opening of the net and the warp tension.

#### 6.1.1 Single Warp Tension ~ W.T.

$$WT = \exp(-0.30524 + 0.3003 * Vn + 0.00027 * W - 0.0036 * d + 1.10046 * D)$$

For 31 data points this formula predicts the warp tension with a standard deviation in proportional error of 0.049 and on average overestimates by 2.6%.

#### 6.1.2 Horizontal Opening ~ Ho (Wing End Spread)

$$Ho = \exp(4.43014 - 0.02302 * Vn - 0.0039 * W + 1.66405 * D - 0.00142 * d)$$

For 20 data points this formula predicts the Horizontal Opening with a standard deviation in proportional error of 0.018 and on average overestimates by 0.1%.

6.1.3 Vertical Opening ~ Vo (Headline Height)

$$Vo = \exp(3.46534 - 0.20779 * Vn + 0.00254 * W - 1.35148 * D - 0.006926 * d)$$

For 23 data points this formula predicts the Vertical Opening with a standard deviation in proportional error of 0.049 and on average underestimates by 0.1%

where Vn = net speed (knots)  
W = warp out (fathoms)  
D = vessel distance (naut. miles)  
d = water depth (fathoms)

6.2 Comparison of Predicted and Recorded Values

Plots of the recorded values and the resulting curves derived from the analysis are shown in Figs. 1 to 11 inclusive.

Tabulated analysed values for nominated net speed values for the tows comprising the trial are given in Tables 1-3 for the average depths of water recorded on that tow. Tabulated predicted results for nominated values of warp, vessel distance, water depth and net speed are given in Tables 4-12.

7            RESULTS

The results of the analysis show that whilst holding the remainder of the variables constant (i.e. to consider net speed; warp, distance and depth remain constant), the effect of:

- (i)        increasing net speed gives ~~over~~ an operating range of 2.4 to 3.8 knots
- a)        increased warp tension at a rate of 35% per knot
- b)        decreased horizontal opening at a rate of 2% per knot
- c)        decreased vertical opening at a rate of 19% per knot
- (ii)       increasing the length of warp out gives
- a)        increased warp tension at a rate of 1.4% per 50 fathoms
- b)        decreased horizontal opening at a rate of 2% per 50 fathoms
- c)        increased vertical opening at a rate of 13.5% per 50 fathoms
- (iii)      increasing the vessel distance apart
- a)        increased warp tension at a rate of 11% per 1/10th nautical mile
- b)        increased horizontal opening at a rate of 16.6% per 1/10th nautical mile
- c)        decreased vertical opening at a rate of 13.5% per 1/10th nautical mile



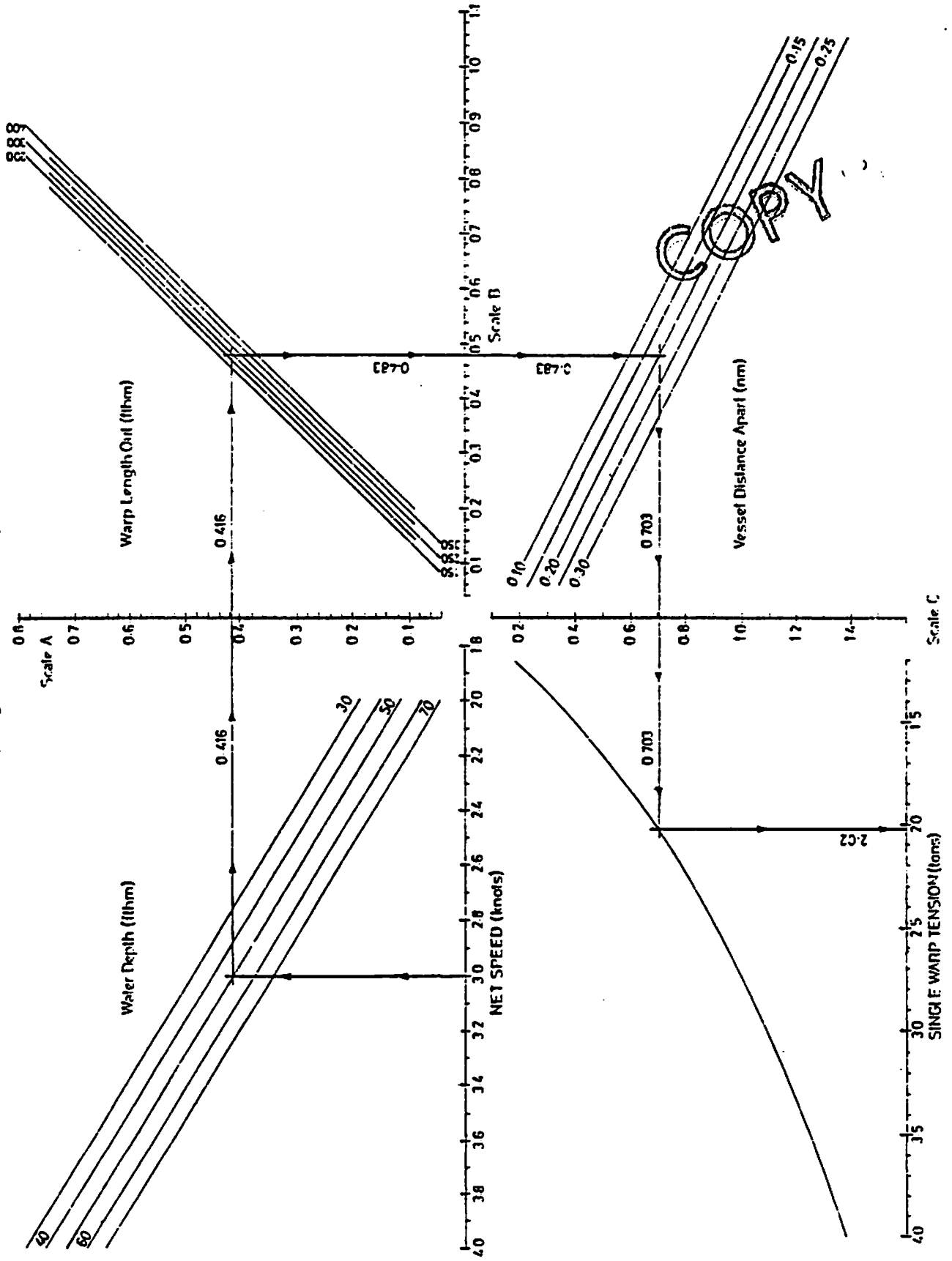
- (iv) increasing water depth gives -
- a) decreased warp tension at a rate of 3.6% per 10 fathoms
  - b) decreased horizontal opening at a rate of 1.4% per 10 fathoms
  - c) decreased vertical opening at a rate of 10.9% per 10 fathoms.

A tabulated summary of these results is given in Table 13.

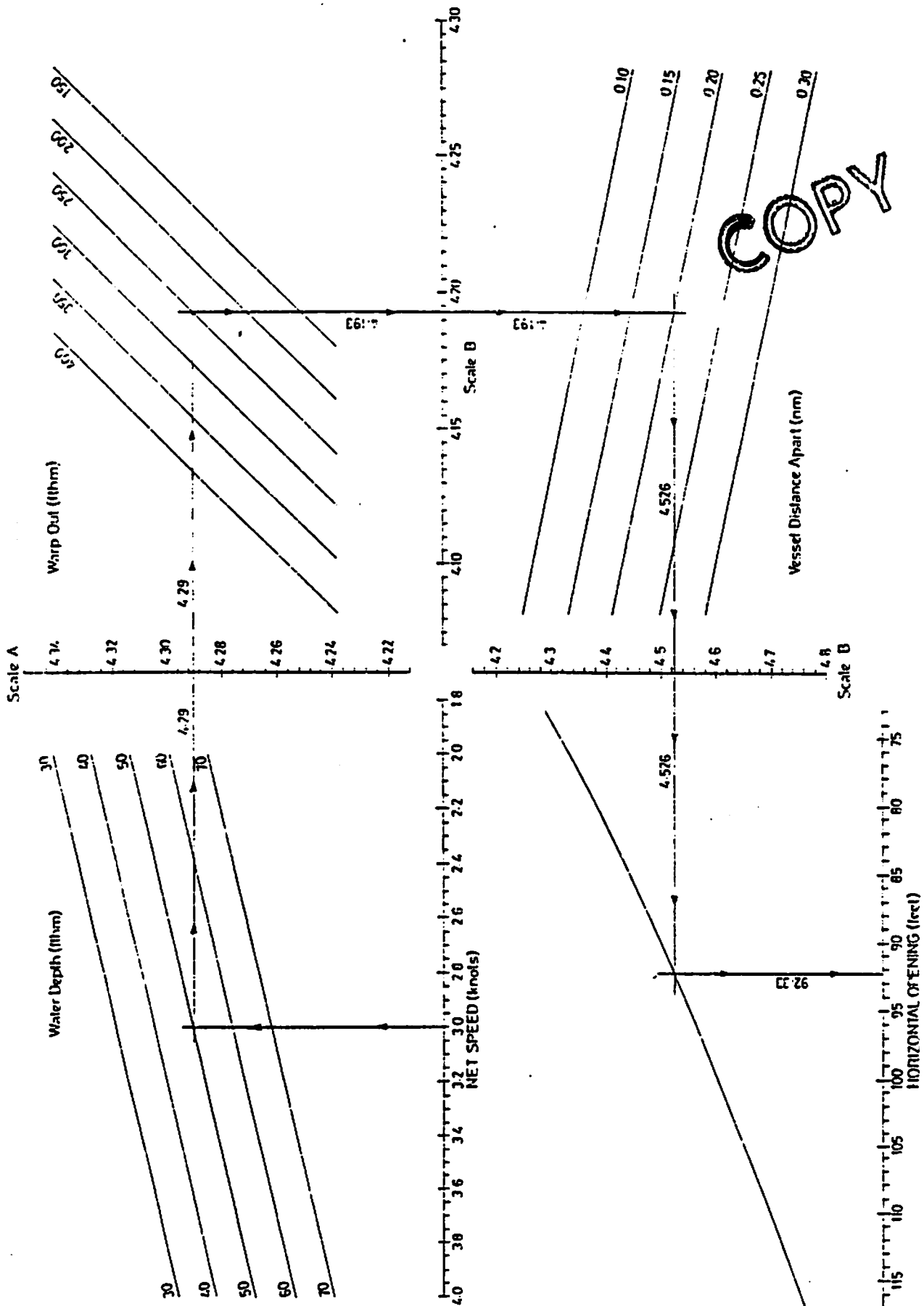
In order that these results may be readily used a graphical method is presented from which the values of warp tension, horizontal opening, and vertical opening can be determined - ref. Figs. 15 to 26.

This presentation is based on the premise that the user is familiar with the grounds he wishes to fish and the type of fish to be caught. Using his knowledge and experience he will know therefore the speed required to catch the fish, the depth of water, and the net setting most suitable for the shoaling characteristics of that type of fish. A summary presentation - comprising three graphs - of Figs. 15 to 26 is given overleaf, and also in Appendix V. A combined cross plot of this data for a typical net speed of 3 knots is also given in Appendix V.

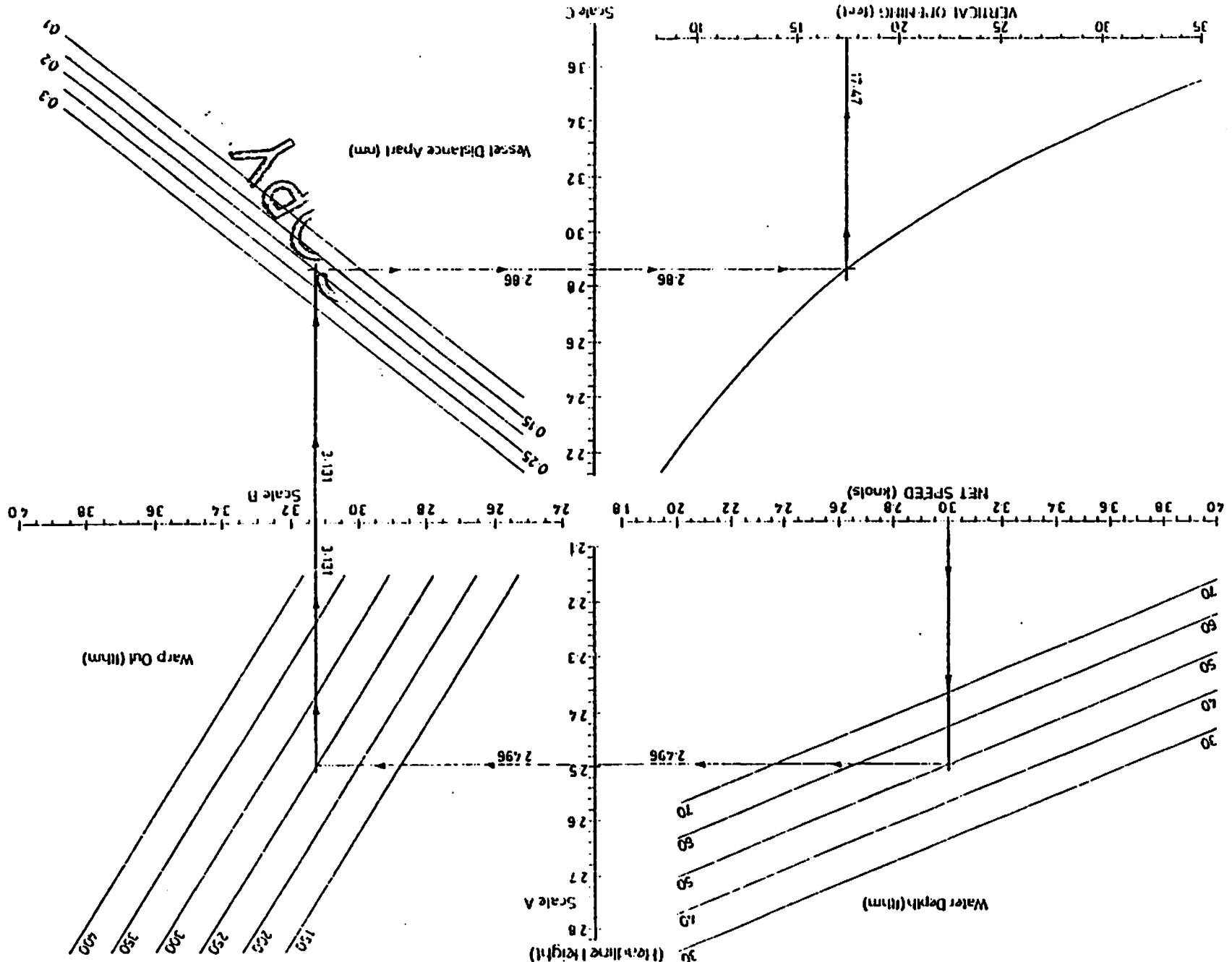
# SINGLE WARP TENSION



# HORIZONTAL OPENING (Wing Error Spread)



# VERTICAL OPENING



8            DISCUSSIONS

8.1        General

When a change in either vertical or horizontal opening is required it can be achieved by changing either vessel speed, warp out, vessel distance apart or a combination of these. The effects of changes in these variables is summarised in Table 13.

If an increase in warp tension is incurred then an increase in fuel consumption is also incurred. The potential increase in catch rate effected by a change in one or more of the above variables must justify the increase in fuel consumption. In order to assist skippers in making decisions which are relative to fuel costs a guide is necessary which relates fuel costs to warp tension. To this end it may be said that:

- (i)        whilst maintaining a constant net speed a change in warp tension of 10% will incur a change in fuel rate of approximately 20% (i.e. varying warp and vessel distance to change warp tension)
  
- (ii)       whilst maintaining constant warp and vessel distance a change in warp tension of 10% will incur a change in fuel rate of approximately 23% (i.e. varying vessel speed)

A tabulated summary of the changes incurred equivalent to a 10% increase in warp tension is given below.

For 10% increase in Warp Tension

Change incurred by	Amount of Change	Approximate % Change		
		Horizontal Opening	Vertical Opening	Fuel Rate
Speed	+ 0.3 knot	- 0.6	- 5.4	+23
Warp	+ 357 fathom	-14.3	+96.4	+20
Vessel Distance	+ 0.09 nm	+15.1	-12.3	+20
Depth	-27.8 fathom	-3.9	+30.3	+20

The vertical and horizontal openings decrease as net speed increases. The natural explanation for this is that as speed increased more of the sweepwire is pulled off the seabed by virtue of increasing the net resistance and this reduces the spreading force contributed by the friction between the sweeps and the seabed. This is in contrast to single boat trawling using trawl doors where higher net speeds usually give greater spreads.

## 8.2 Horizontal Opening

The horizontal opening decreases as speed, warp and water depth increases and increases as vessel distance increases. Referring to Table 13 it can be seen that in order to increase the horizontal opening an increase in vessel distance is the most efficient option.

e.g. to increase the horizontal opening by 15.1% the vessel distance should be increased by 0.09nm which incurs an increase in fuel rate of 20% and a decrease in vertical opening of 12.3%.

## 8.3 Vertical Opening

The vertical opening increases as warp increases and decreases as speed, vessel distance or water depth increases. Referring to the table above it can be seen that if a change in the vertical opening is required it is best achieved by either increasing the amount of warp out or by decreasing the vessel distance. To increase the vertical opening by 12.3% (a 10% increase in WT incurred) by either:-

increasing warp by 45 fathoms which would increase the fuel rate by 2.6% and decrease the horizontal opening by 1.8%

or

decreasing the vessel distance by 0.09nm which would decrease the fuel rate by 20% and also decrease the horizontal opening by 15.1%.

Thus it may be said that for a similar increase in vertical opening a fuel rate decrease of 20% and decrease in horizontal opening of 15.1% must be compared with a fuel increase of 2.6% and decrease in horizontal opening together with the unquantifiable effect extra warp would have on herding the fish.

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9            **CONCLUSIONS**

9.1        **Horizontal Opening**

The most effective and efficient method of changing the horizontal opening is by varying the distance apart of the vessels. Adjustments to the warp out or the speed of the vessel must be quantified in other terms to substantiate their use to change the horizontal opening. The effect of a change in depth is minimal -1.4% per 10 fathoms - and therefore a substantial change in depth is necessary to warrant an adjustment being made.

9.2        **Vertical Opening**

To effect a change in vertical opening the most effective method is a choice between changing the amount of warp out or changing the vessel distance. The former incurs little change in fuel consumption and horizontal opening but has an unquantifiable effect of warp on fish herding. The latter has a substantial effect on both fuel consumption and horizontal opening. The effect of a change in depth is also quite substantial - 30% per 10 fathoms and therefore adjustments to the vessel distance or warp out may be necessary when fishing on a shoaling tow.

9.3        **Vessel Speed**

A change in vessel speed to improve fishing effort must be used with caution since an increase in speed whilst only marginally effecting the set of the nets, does so negatively and incurs a substantial increase in fuel rate.

#### 9.4 Warp

A change in the amount of warp out will incur a substantial change in vertical opening whilst giving only small changes in horizontal opening and fuel costs.

#### 9.5 Vessel Distance

Changing the vessel distance is the most effective way of changing the set of the net. It does however give a greater percentage change in fuel rate than it does on either vertical or horizontal opening.

#### 9.6 Water Depth

A variation in water depth substantially affects both the vertical opening and fuel rate. However, as depth changes the effects on vertical opening and fuel rate, in terms of efficiency, oppose each other.

# SINGLE WARP TENSION ~ 175ftm WARP

Ave. Mean Water Depth 18.67ftm

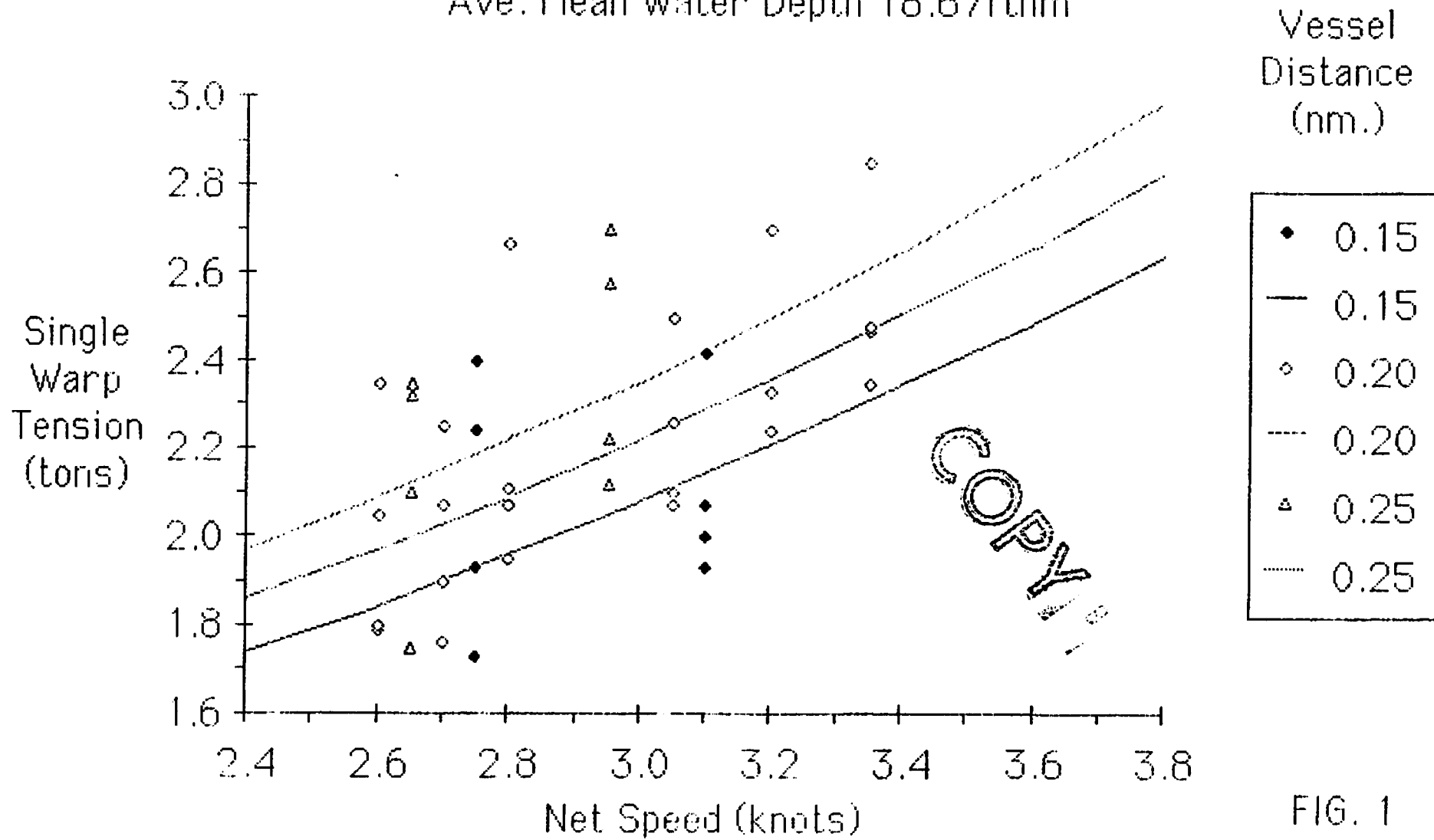


FIG. 1

# SINGLE WARP TENSION ~ 250fthm WARP

Ave. Mean Water Depth 51.03fthm

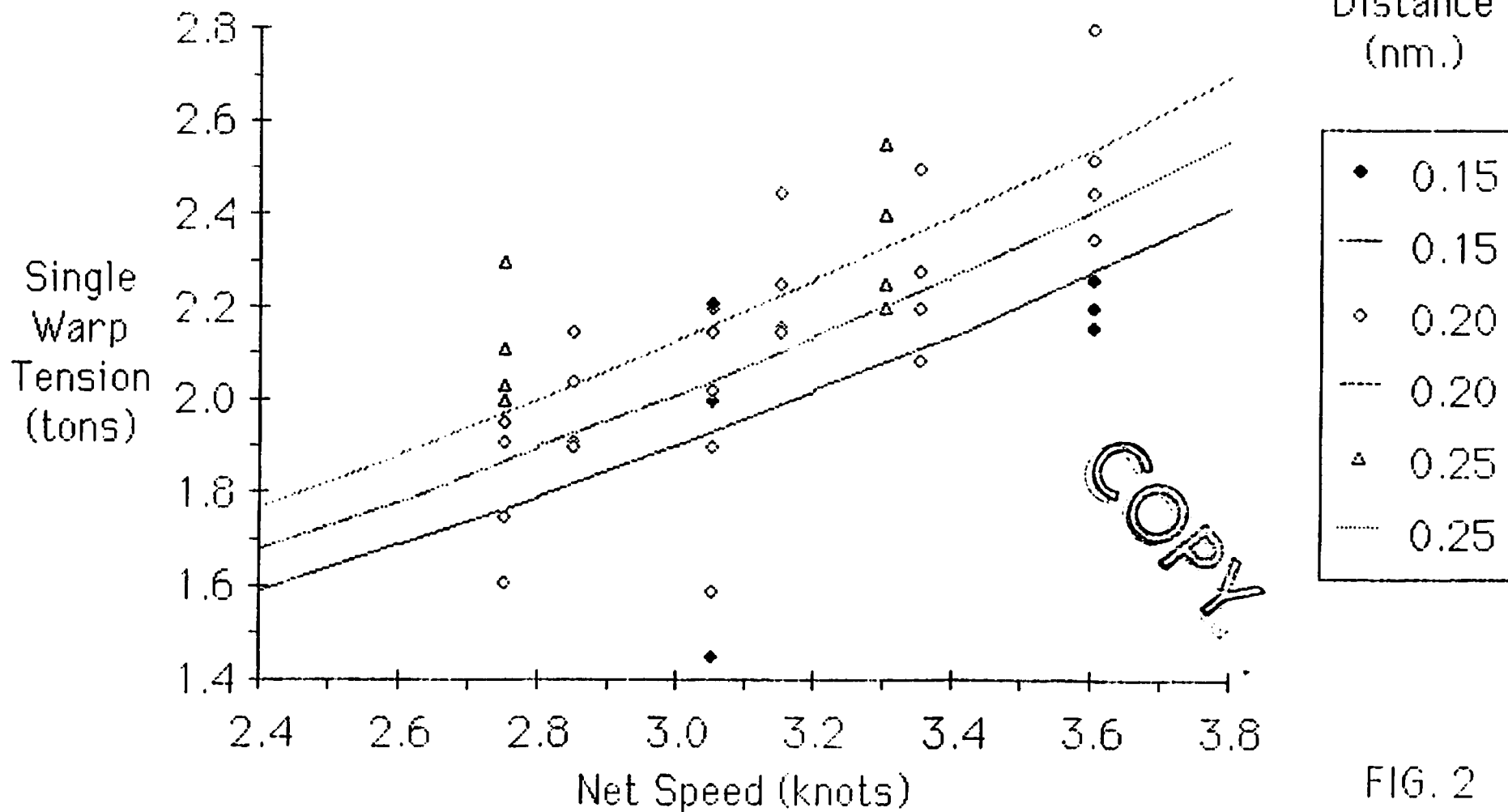


FIG. 2

# SINGLE WARP TENSION ~ 300fthm WARP

Ave. Mean Water Depth 50.75fthm

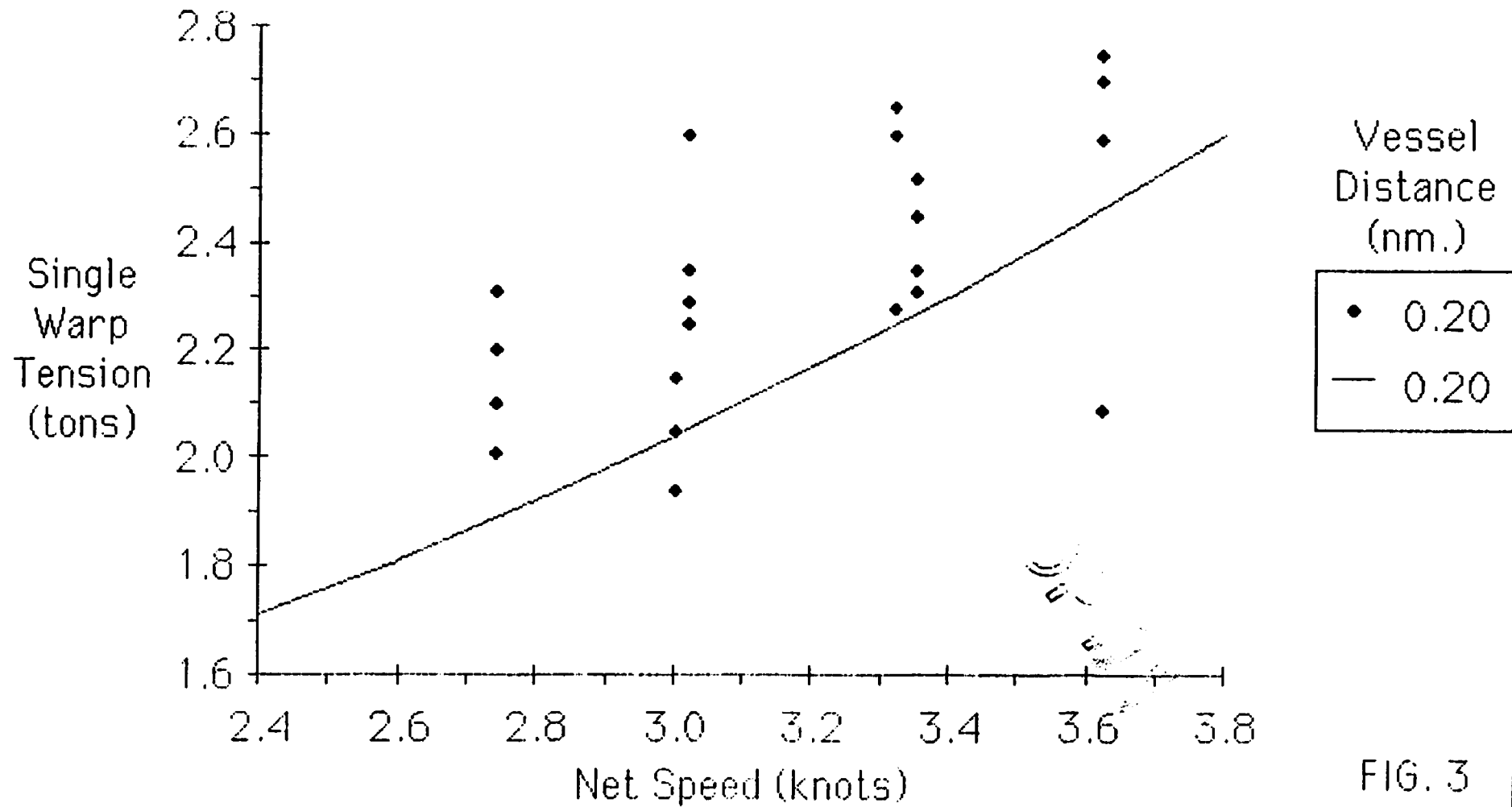


FIG. 3

# SINGLE WARP TENSION ~ 350fthm WARP

Ave. Mean Water Depth 55.16fthm

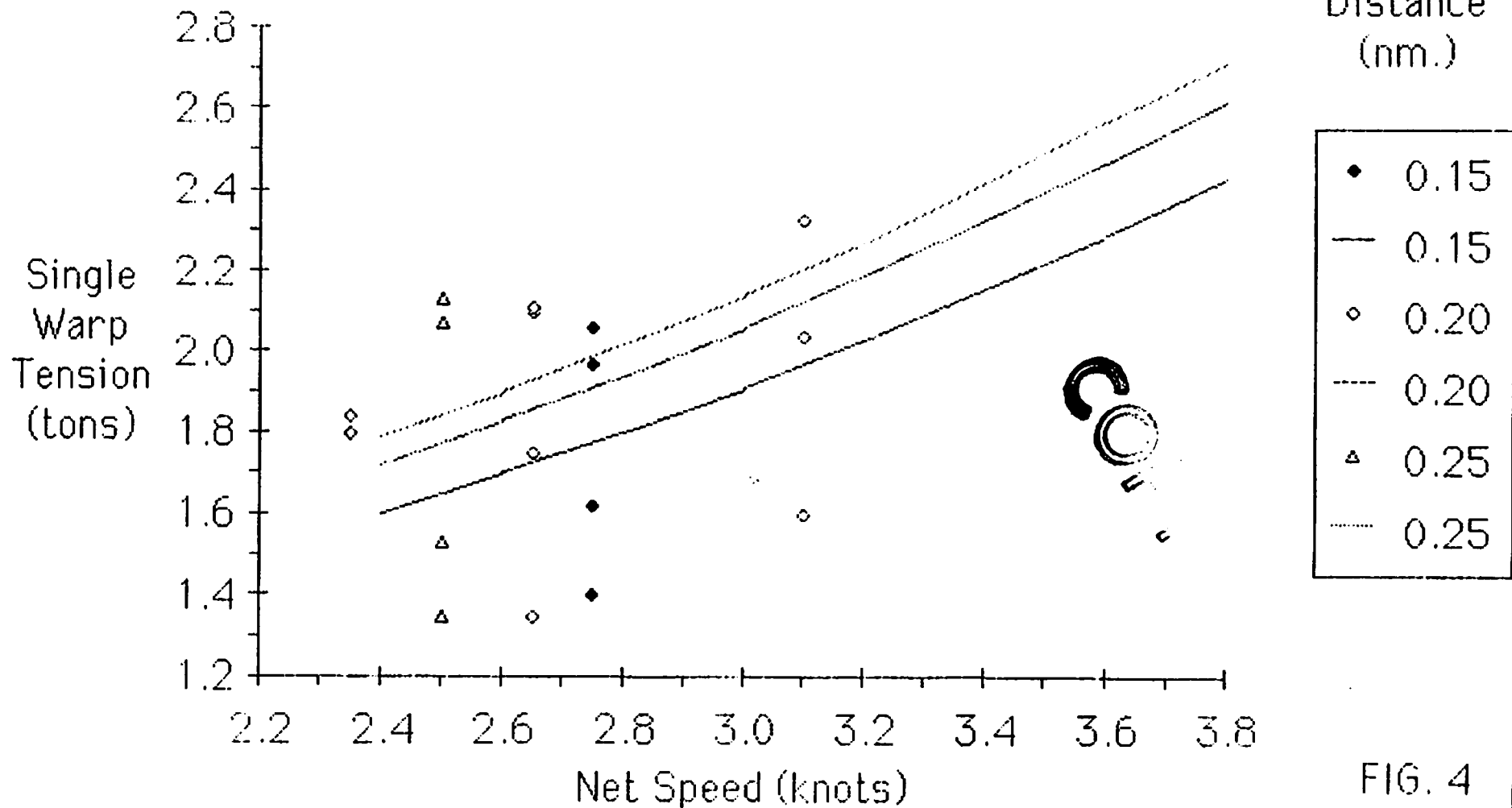


FIG. 4

HORIZONTAL OPENING ~ 175ftlm WARP  
(WING END SPREAD)  
Ave. Mean Water Depth 18.67ftlm

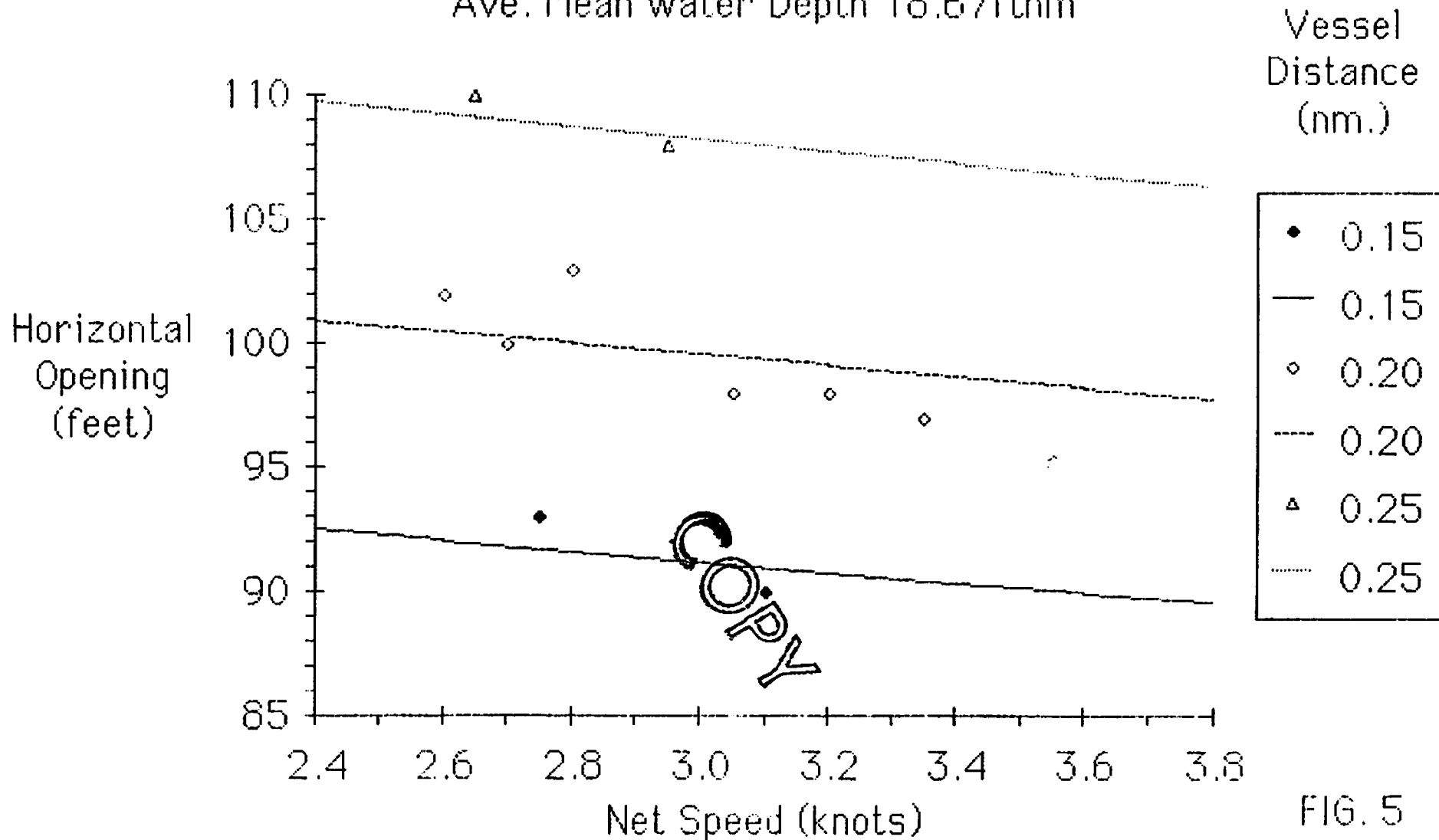


FIG. 5

HORIZONTAL OPENING ~250fthm WARP  
(WING END SPREAD)  
Ave. Mean Water Depth 50.67fthm

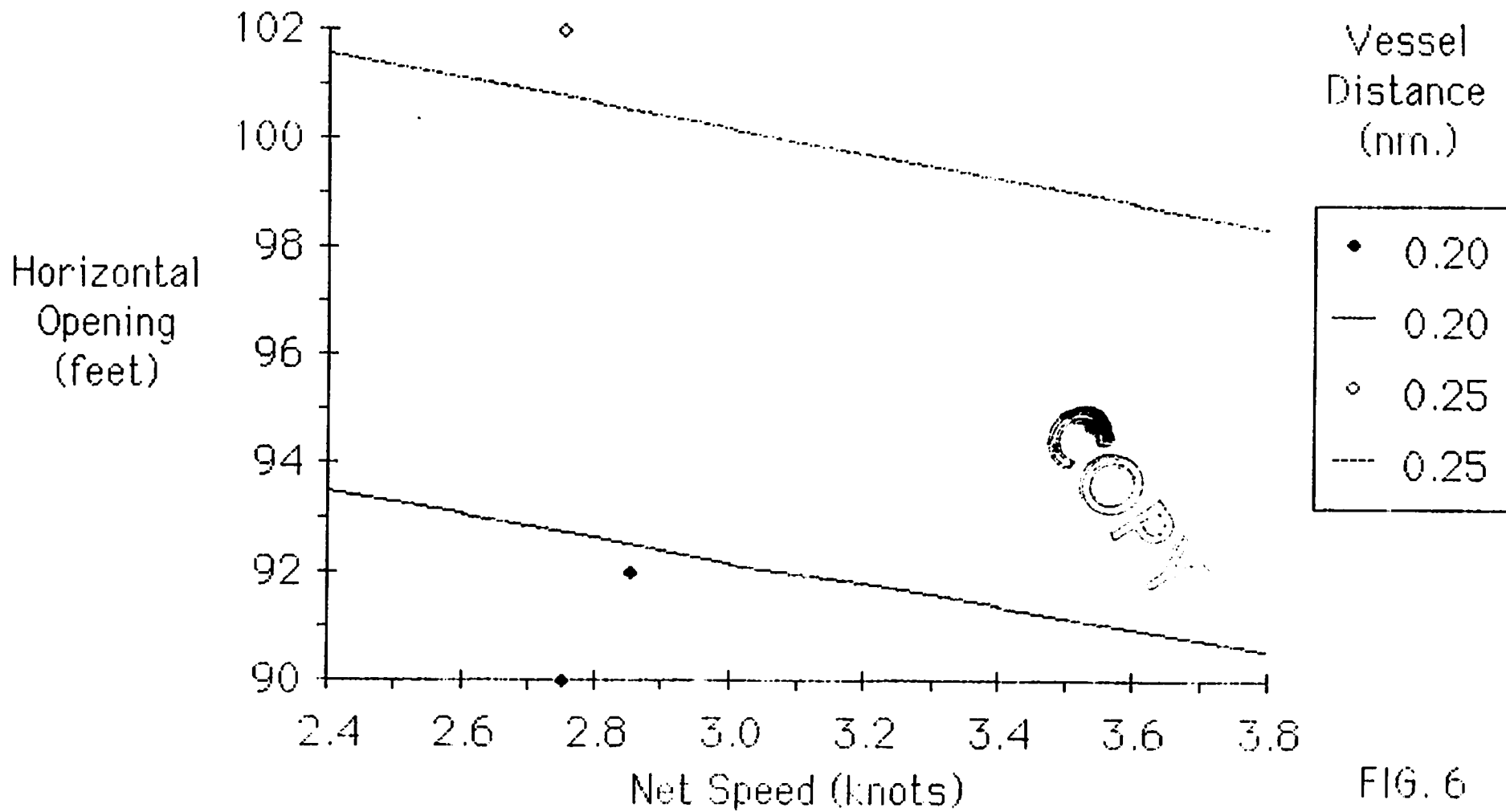


FIG. 6



HORIZONTAL OPENING ~300fthm WARP  
(WING END SPREAD)  
Ave. Mean Water Depth 50.75fthm

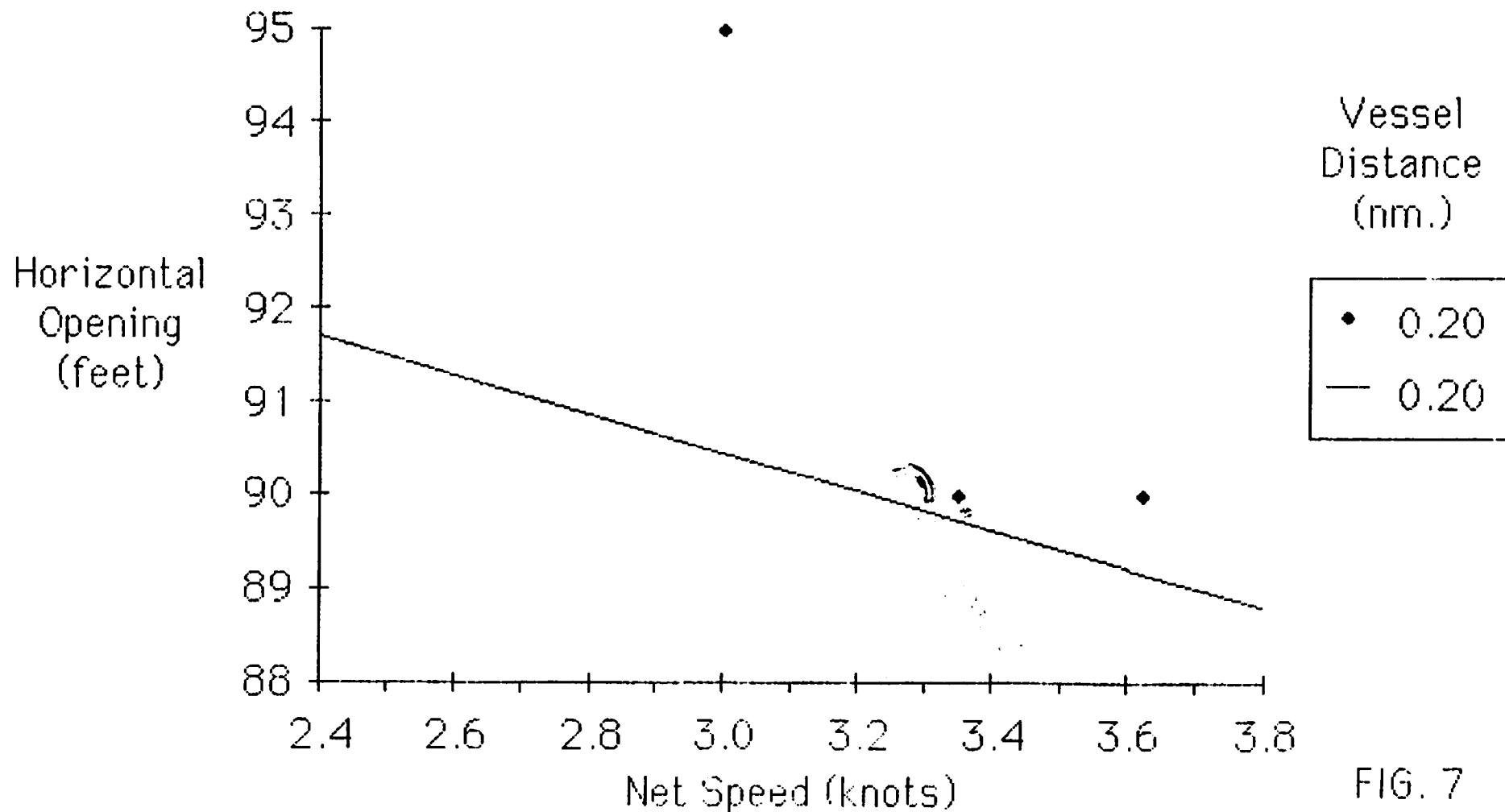
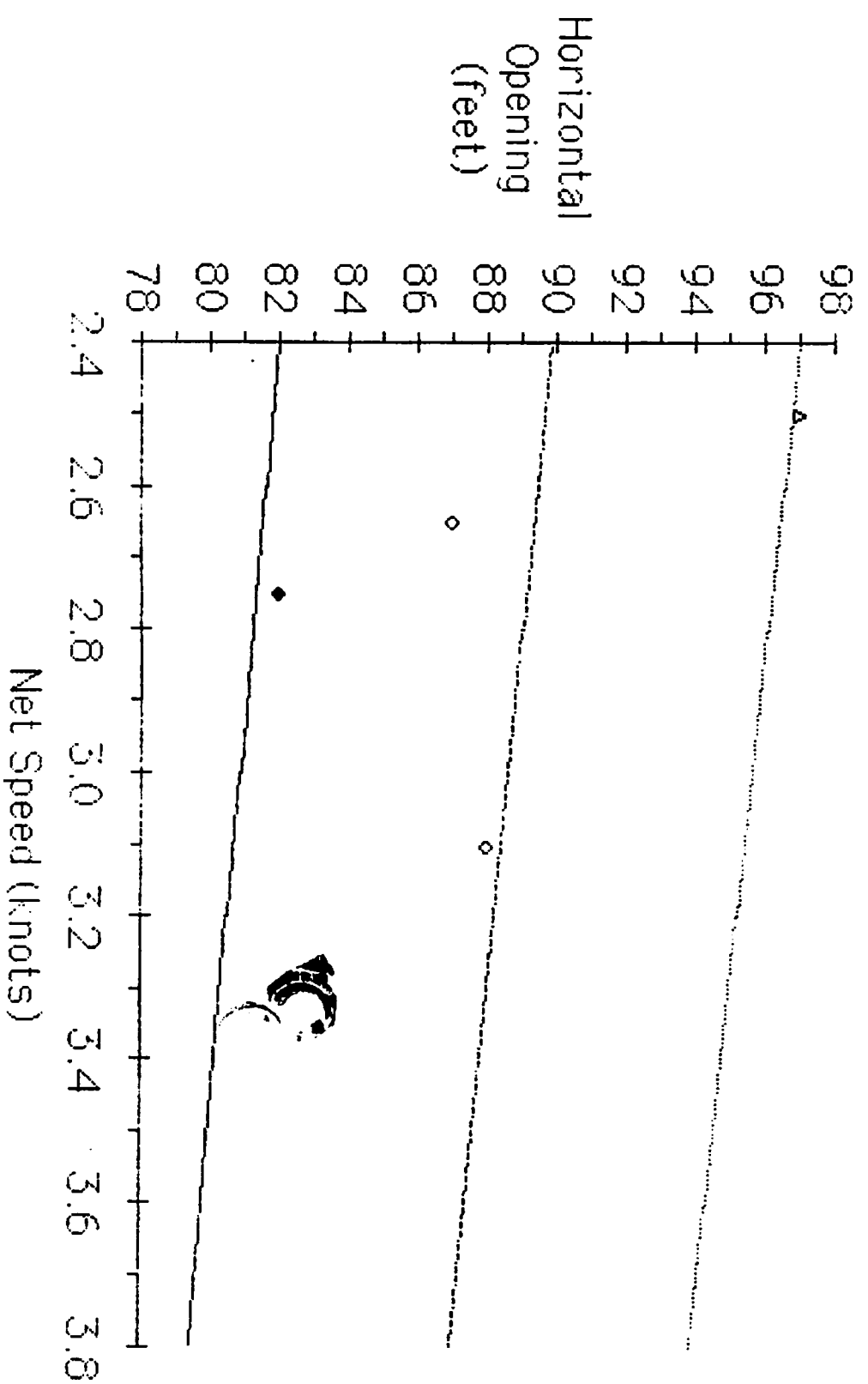


FIG. 7

# HORIZONTAL OPENING ~ 350ftm WARP (WING END SPREAD) Ave. Mean Water Depth 55.16ftm



Vessel  
Distance  
(nm.)

- ◆ 0.15
- 0.15
- ◇ 0.20
- - - 0.20
- △ 0.25
- ..... 0.25

Net Speed (knots)

FIG. 8

# VERTICAL OPENING ~ 175fthm WARP

Ave. Mean Water Depth 18.67fthm

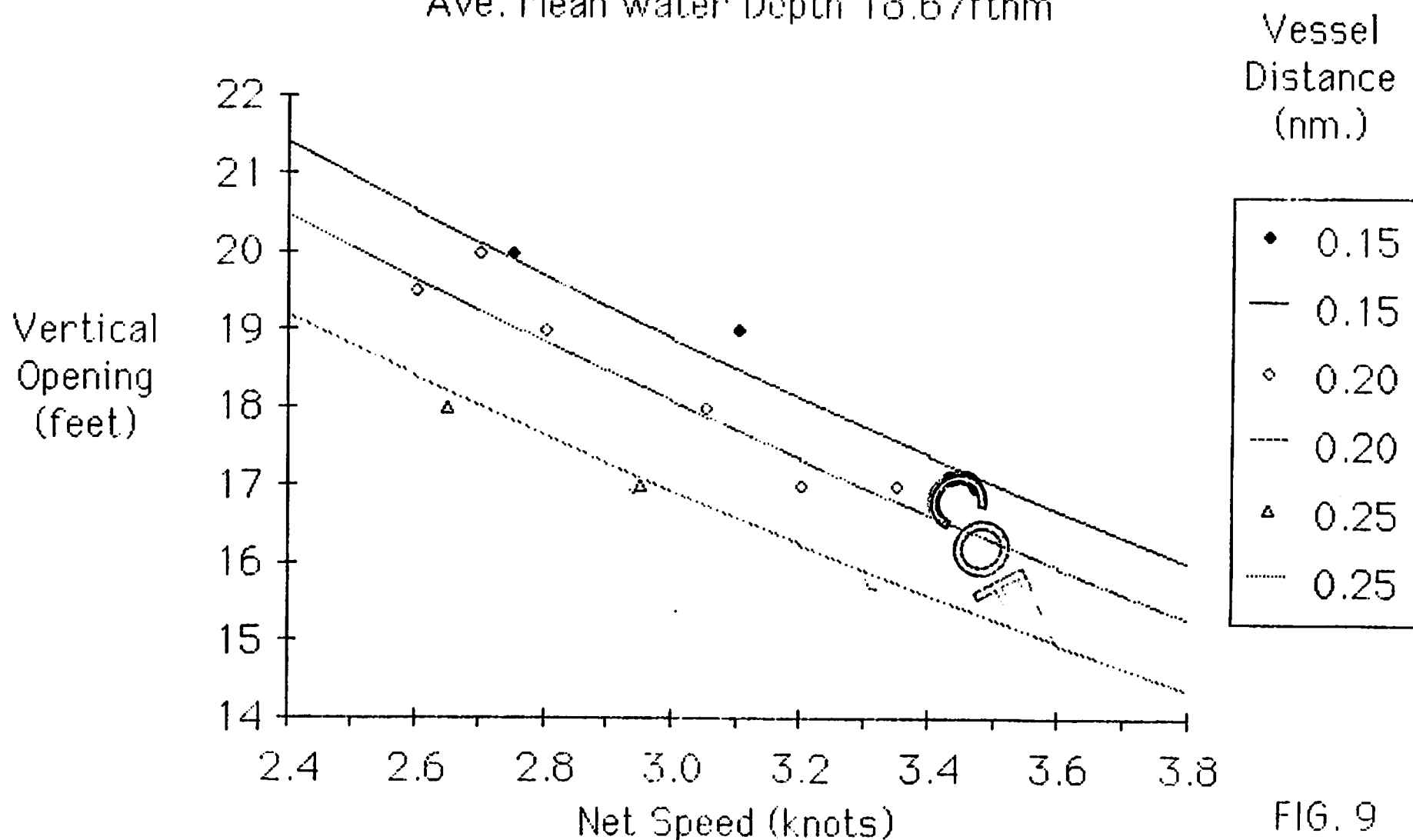


FIG. 9

# VERTICAL OPENING ~250fthm WARP

Ave. Mean Water Depth 51.03fthm

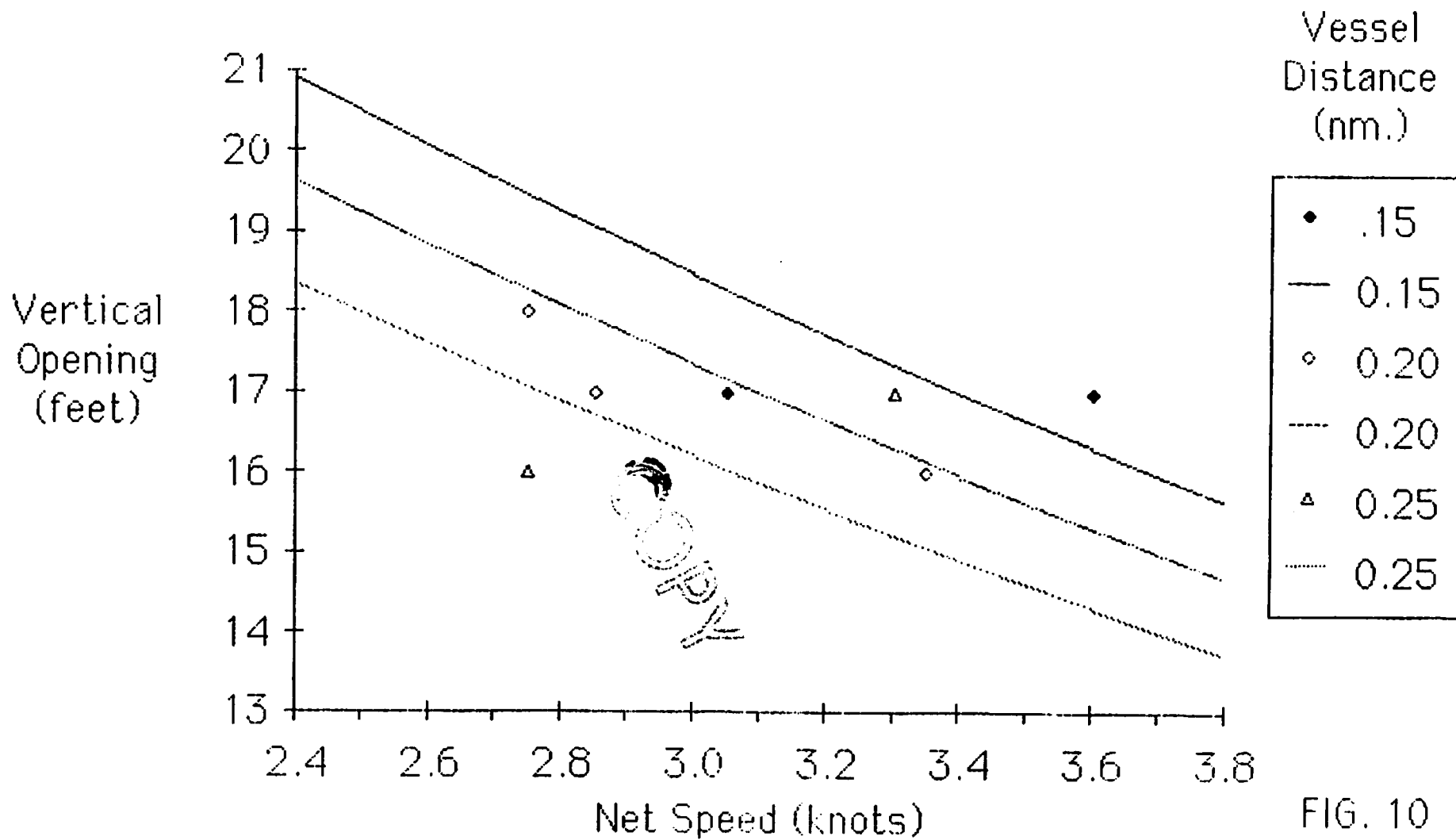


FIG. 10

# VERTICAL OPENING ~350fthm WARP

Ave. Mean Water Depth 55.16fthm

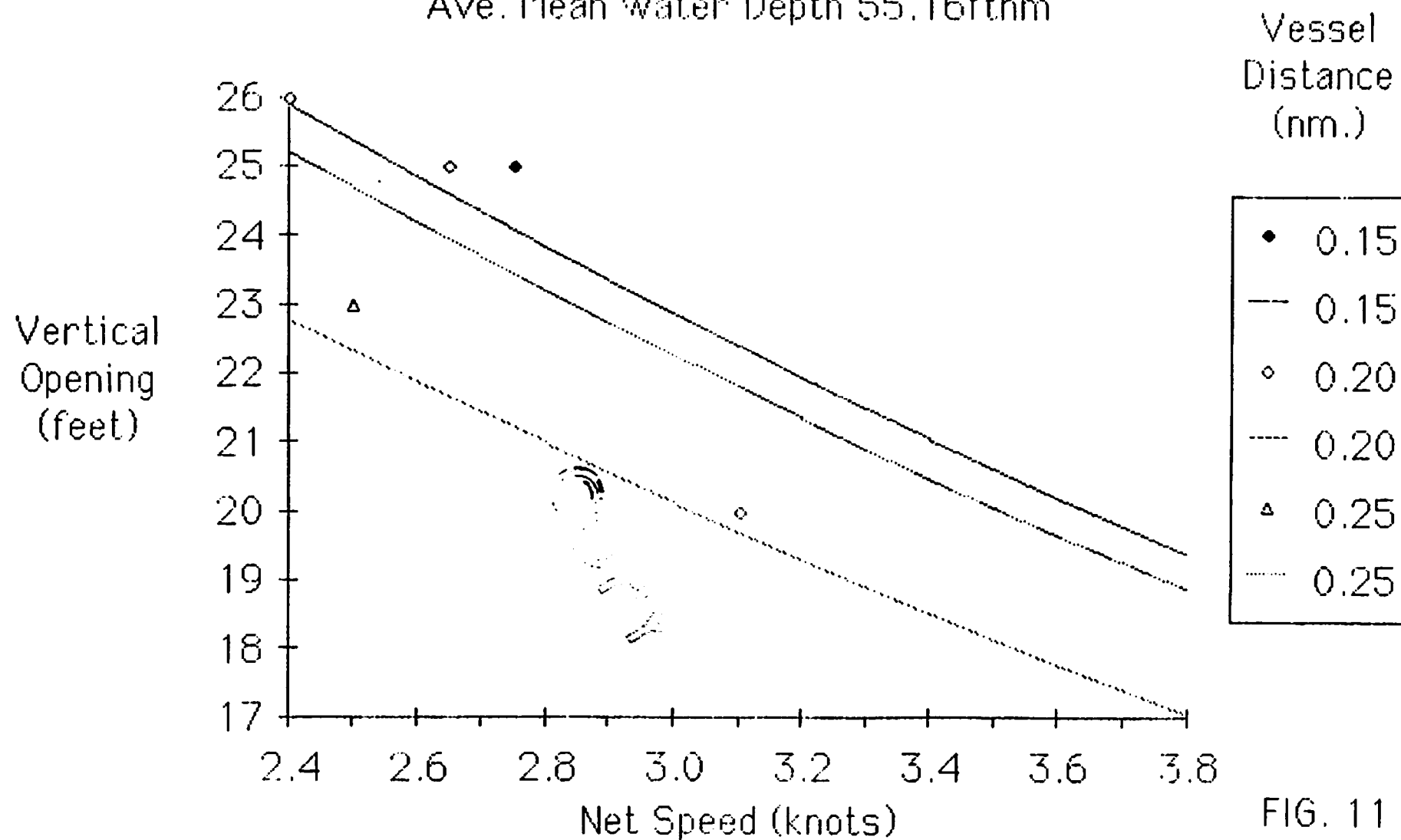


FIG. 11

# SINGLE WARP TENSION

## Comparing recorded & Predicted Values

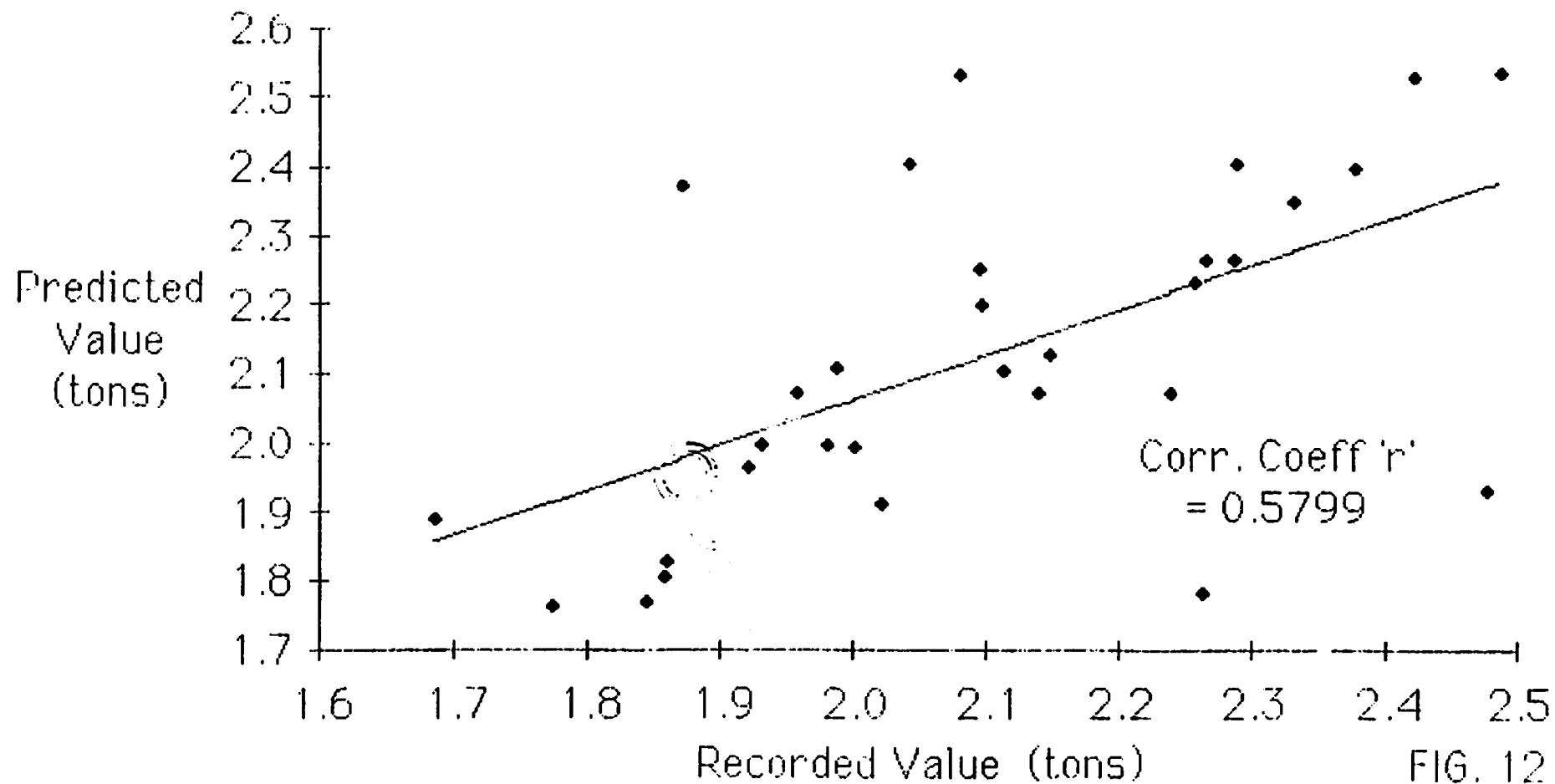


FIG. 12

# HORIZONTAL OPENING

## Comparing recorded & Predicted Values

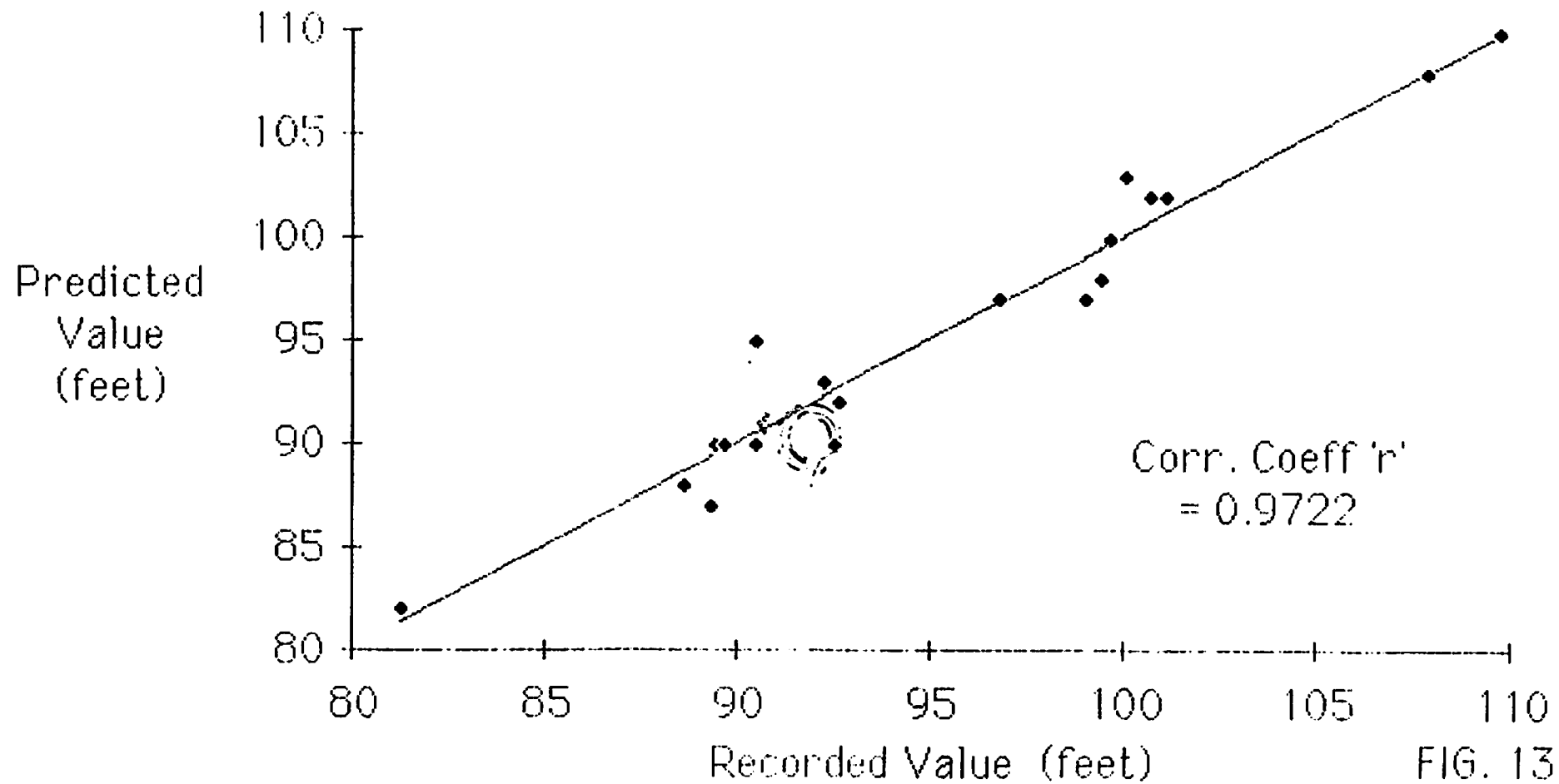


FIG. 13

# VERTICAL OPENING (Comparing recorded & Predicted Values

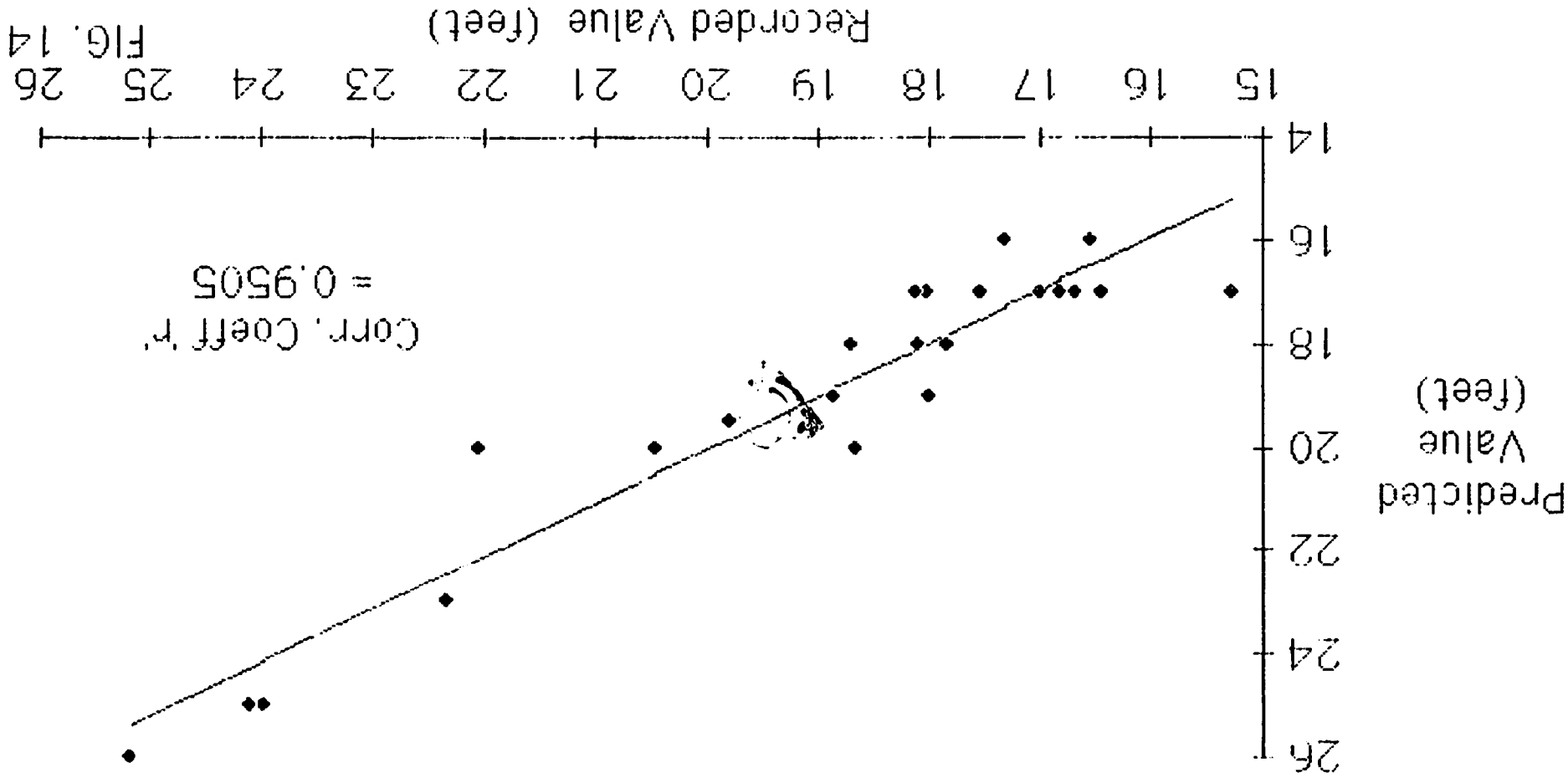


FIG. 14



# SINGLE WARP TENSION

Scale  
'A'

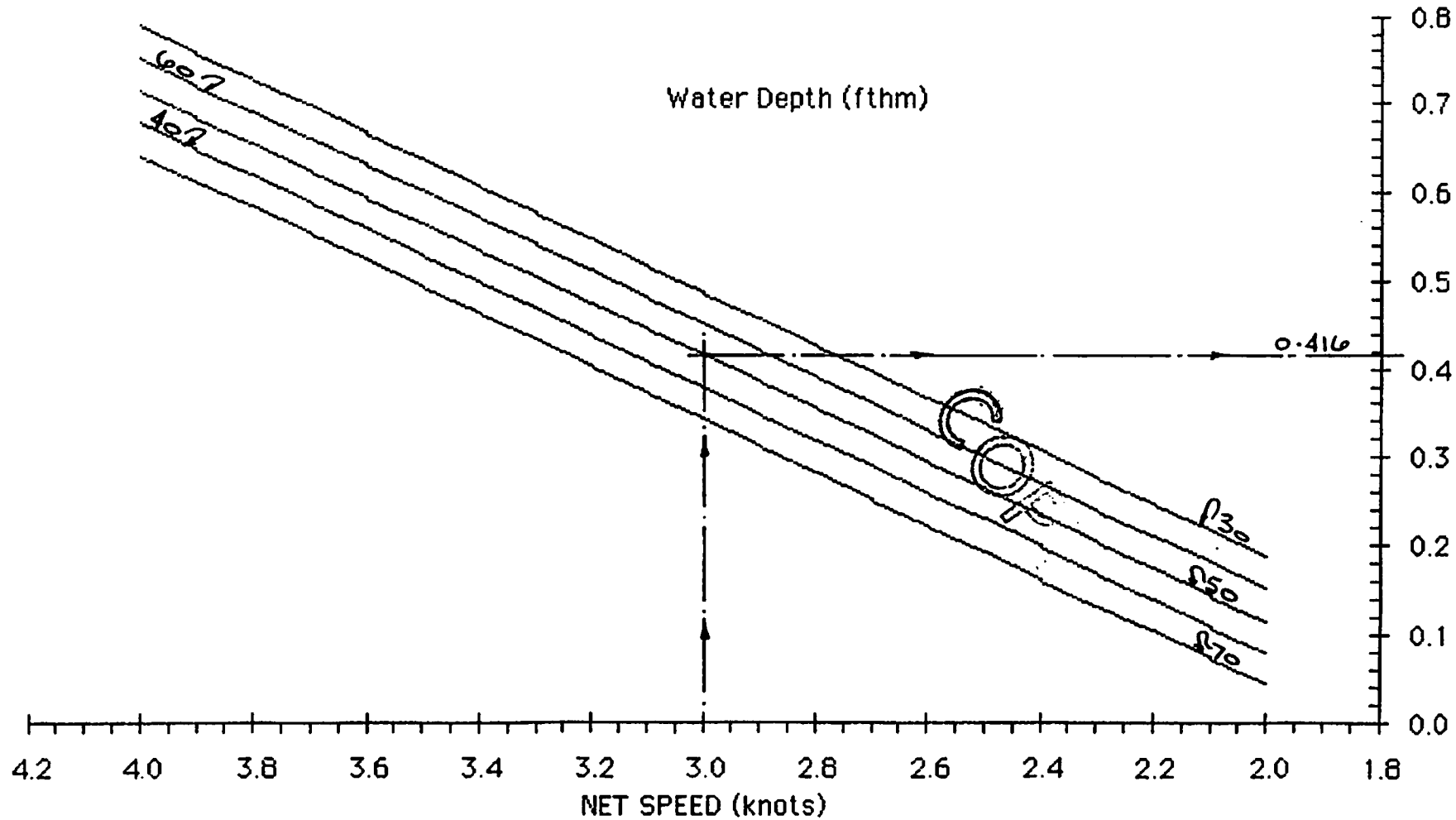


Fig. L5

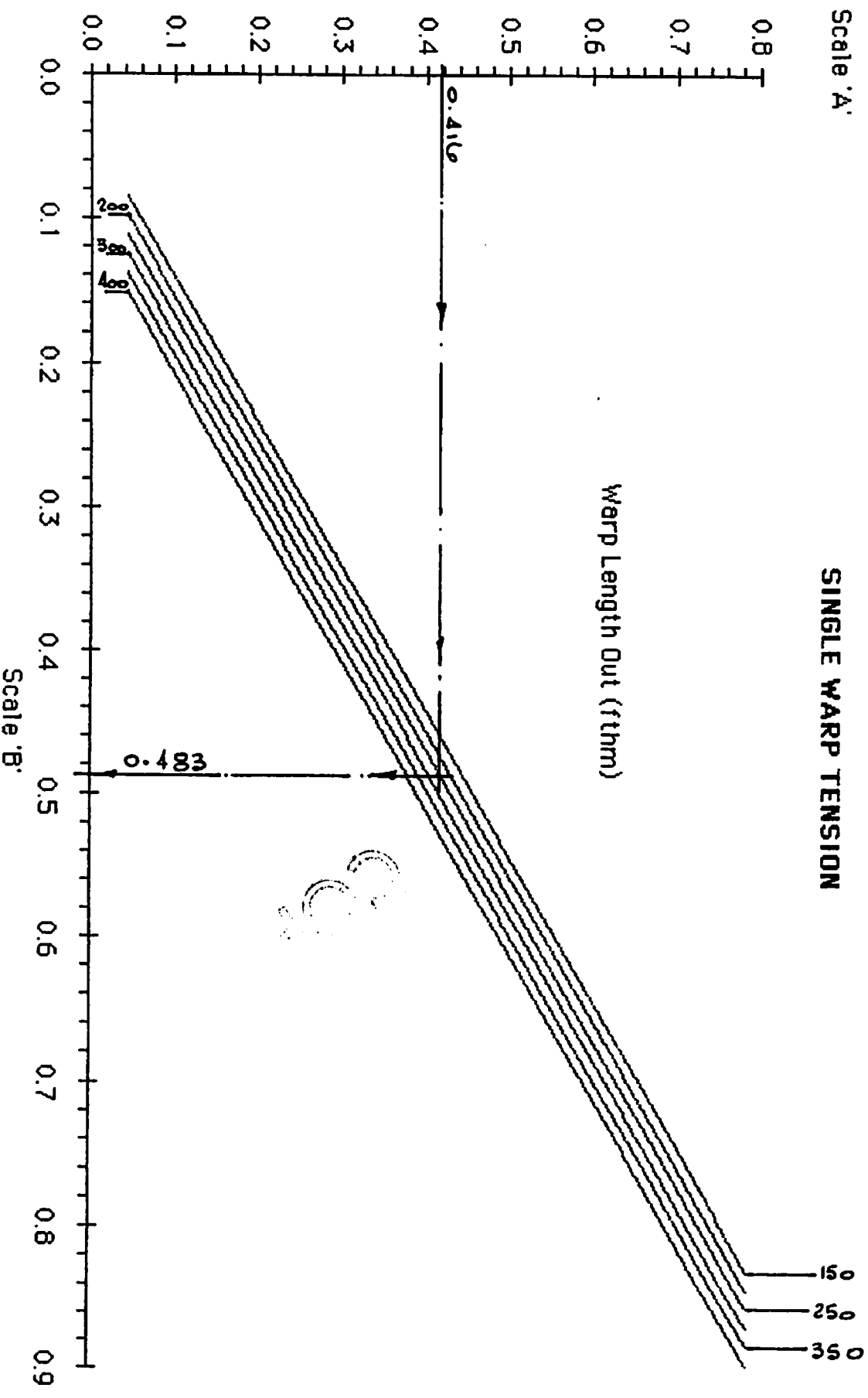


Fig. 16

# SINGLE WARP TENSION

Scale 'B'

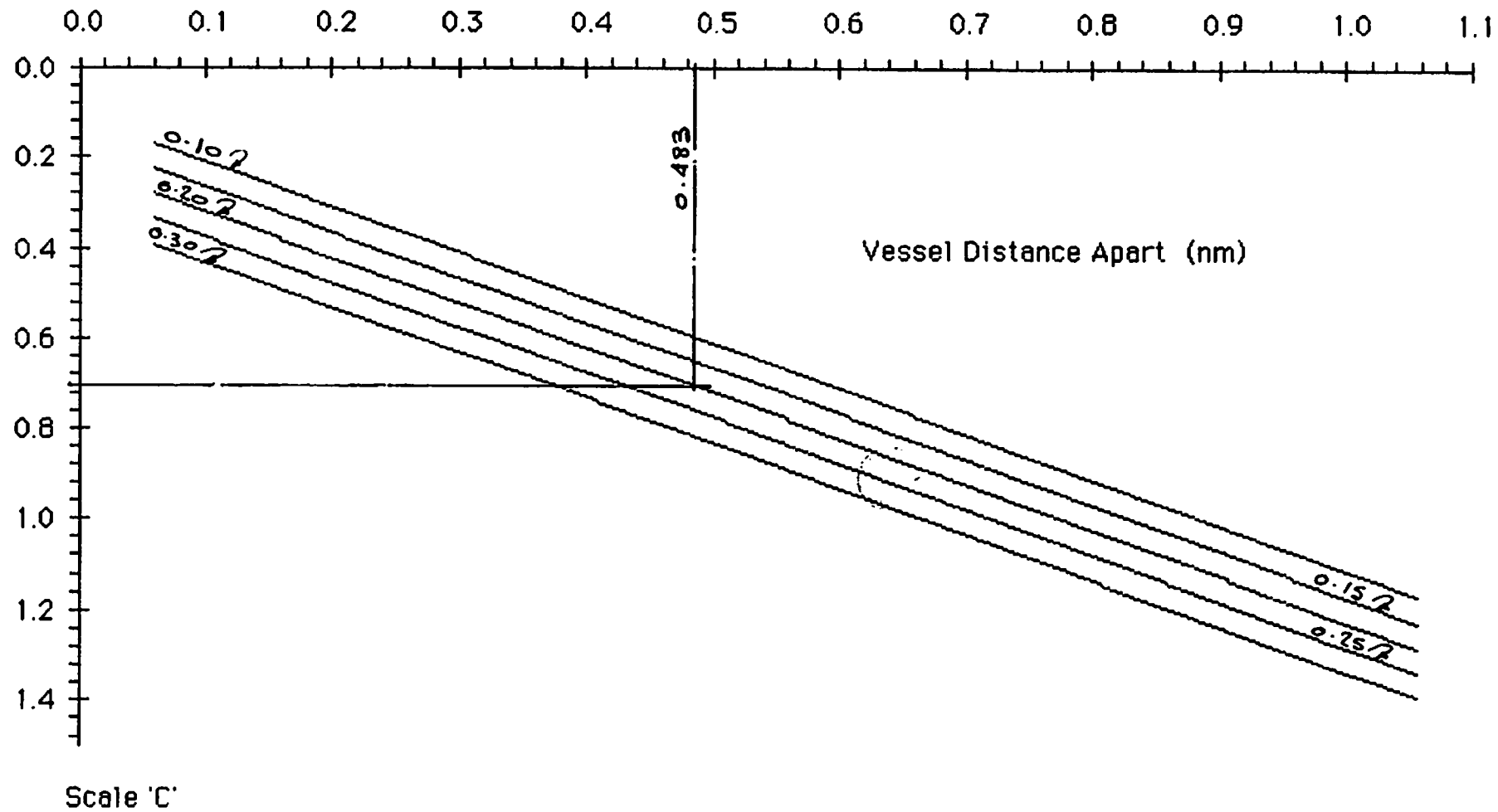


Fig. 17

# SINGLE WARP TENSION

Scale 'C'

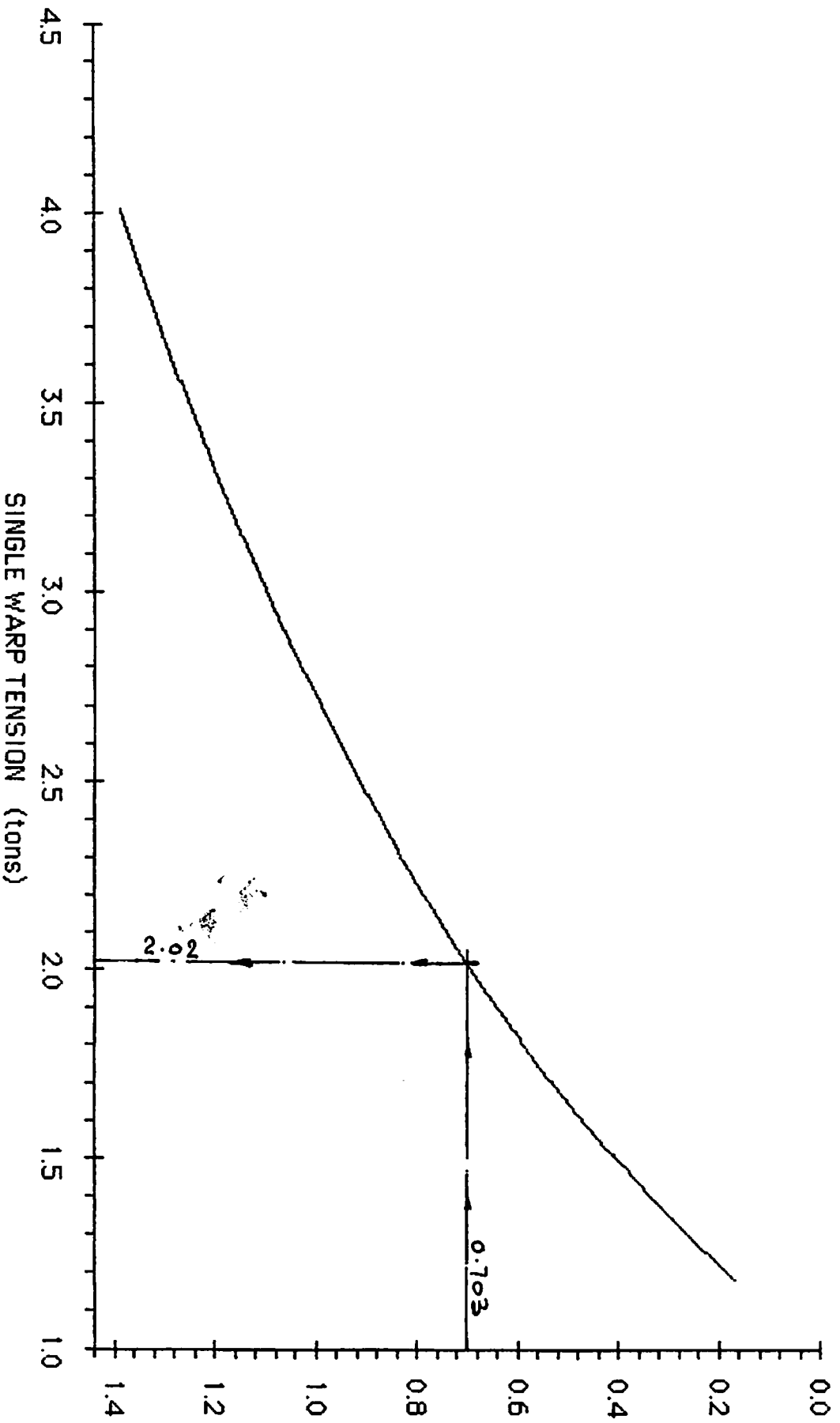


Fig. 18

# HORIZONTAL OPENING (Wing End Spread)

Scale  
'A'

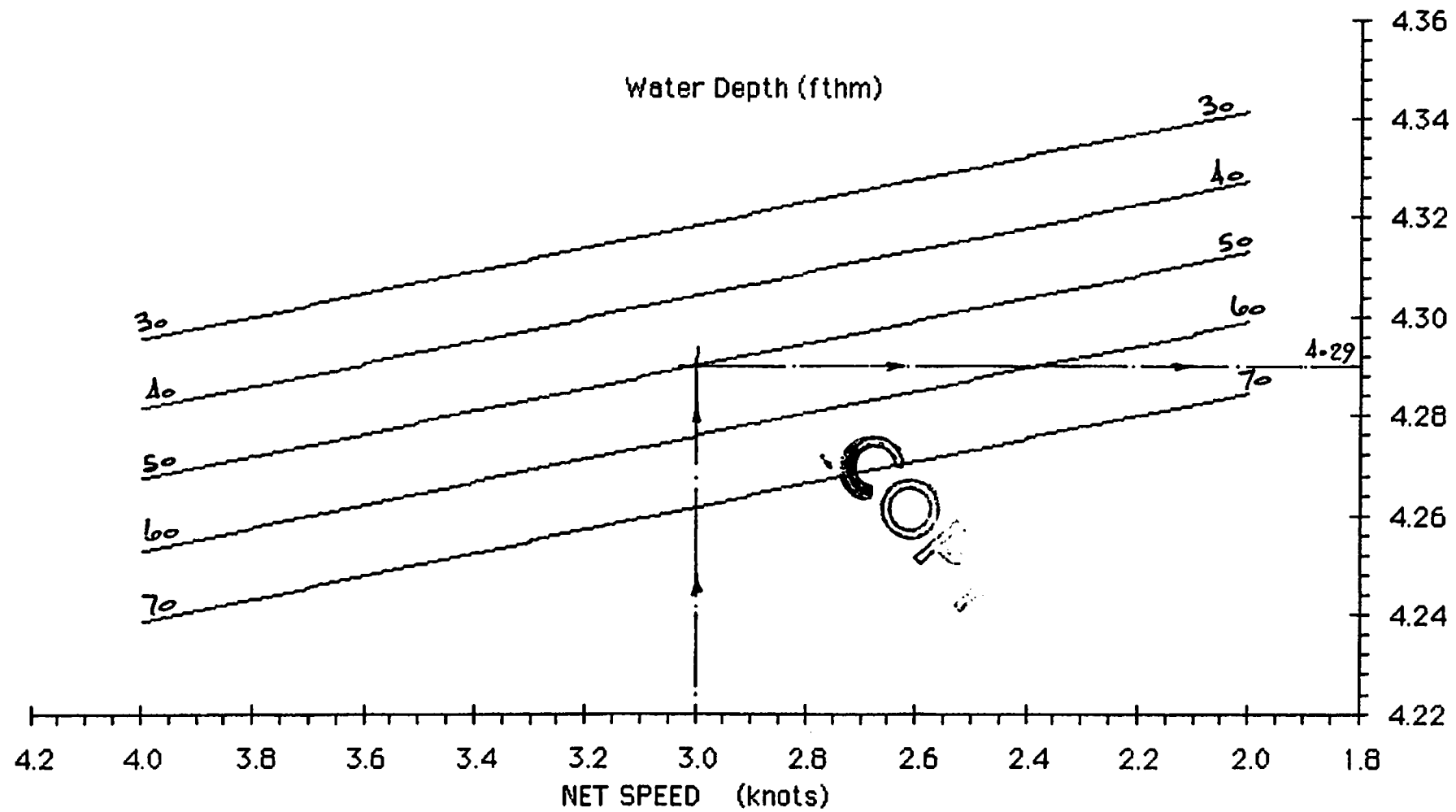


Fig. 19

# HORIZONTAL OPENING (Wing End Spread)

Scale 'A'

4.36  
4.34  
4.32  
4.30  
4.28  
4.26  
4.24  
4.22

Warp Out (fthm)

400  
350  
300  
250  
200  
150

4.29

4.193

4.05

4.10

4.15

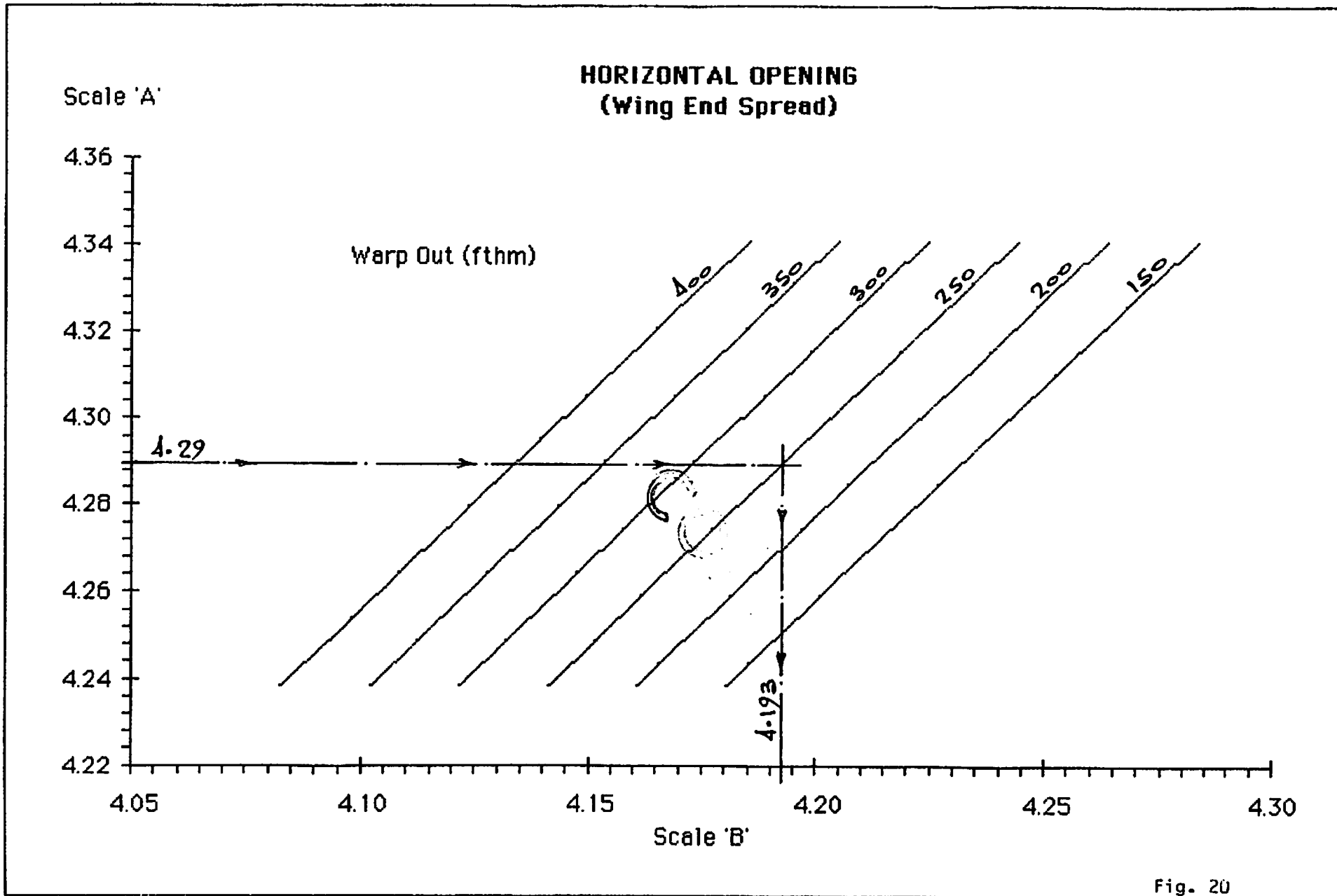
4.20

4.25

4.30

Scale 'B'

Fig. 20



# HORIZONTAL OPENING (Wing End Spread)

Scale 'B'

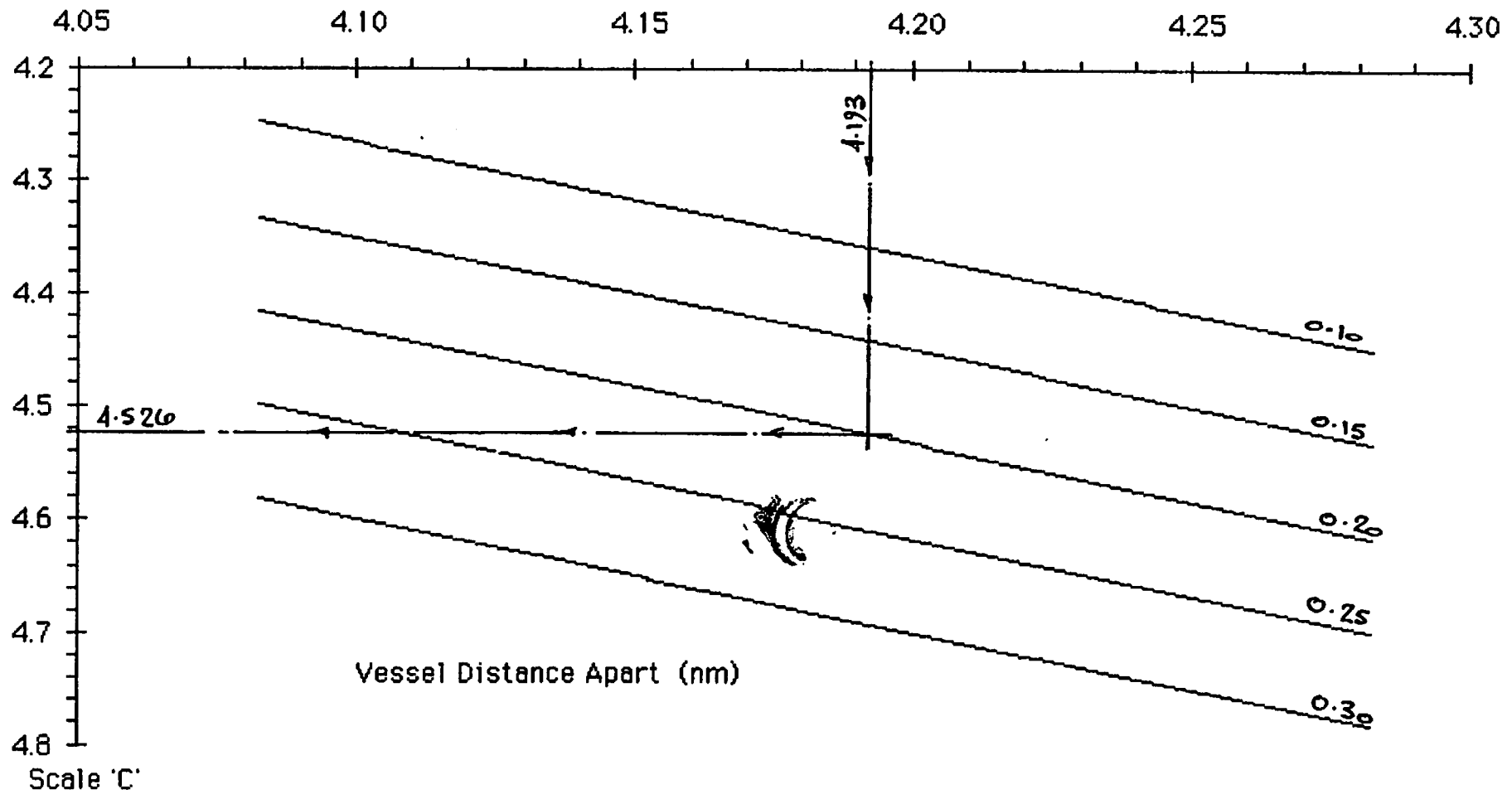
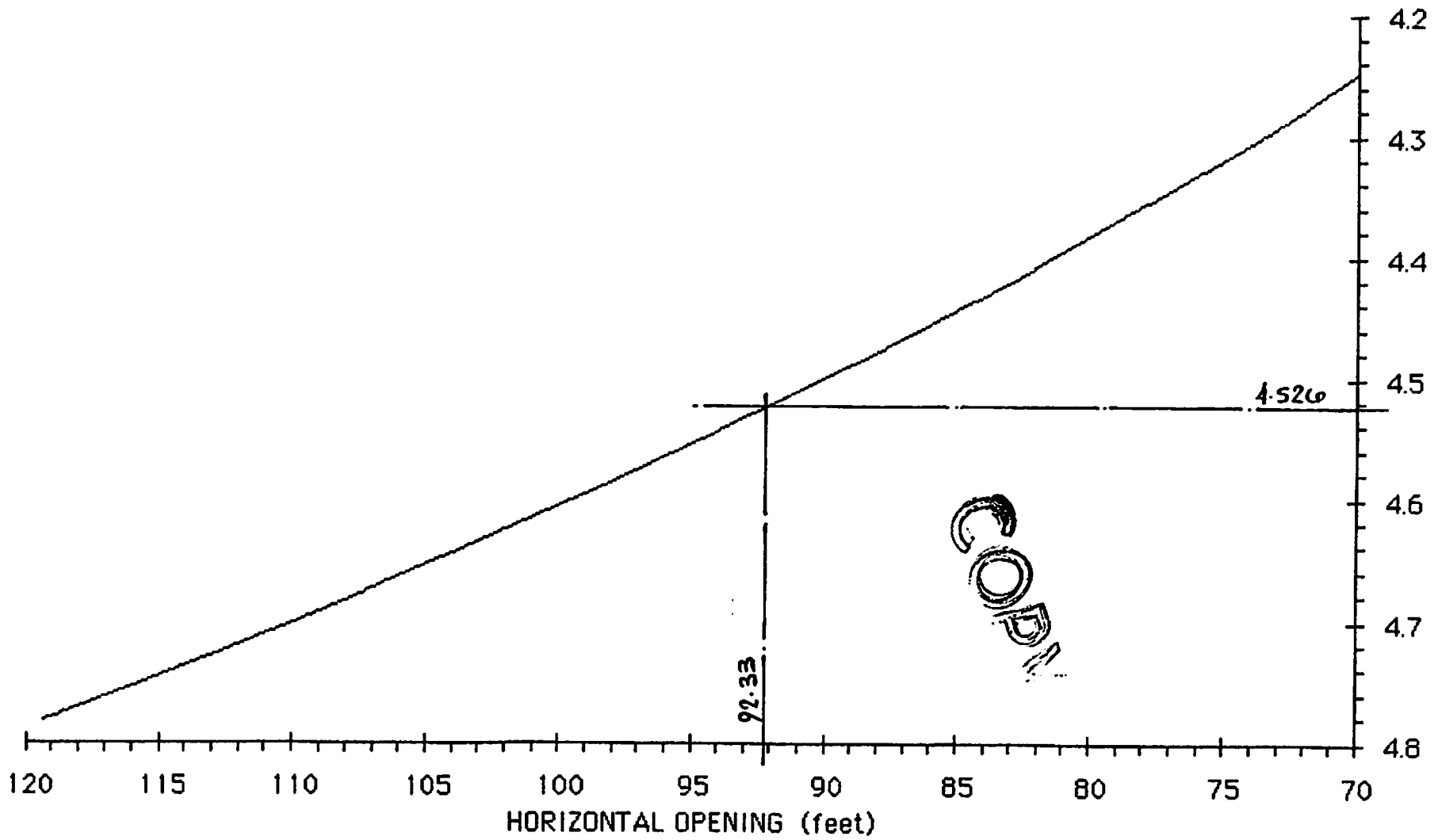


Fig. 21

**HORIZONTAL OPENING  
(Wing End Spread)**

Scale 'C'



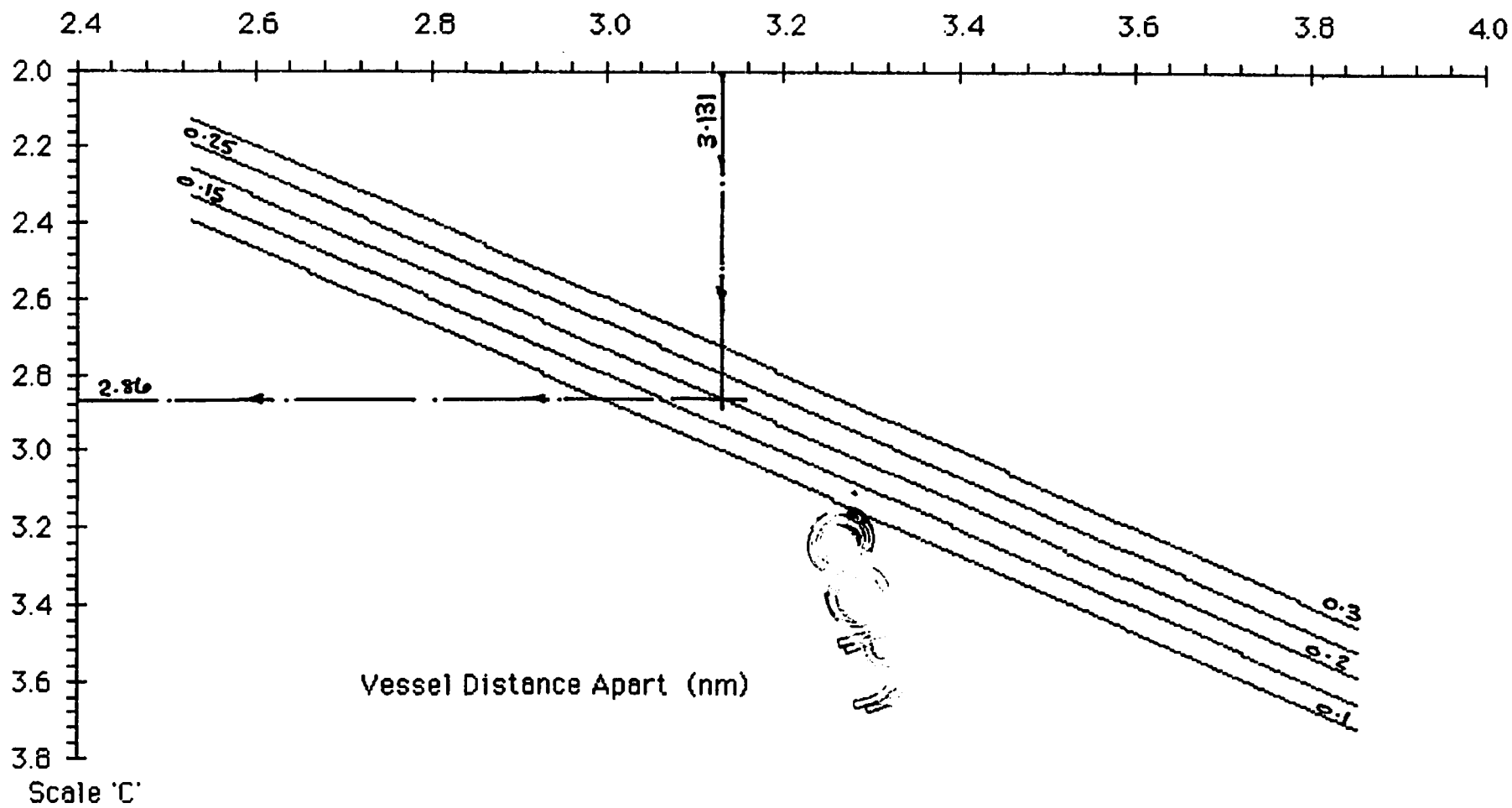
COPY

Fig. 22



# VERTICAL OPENING

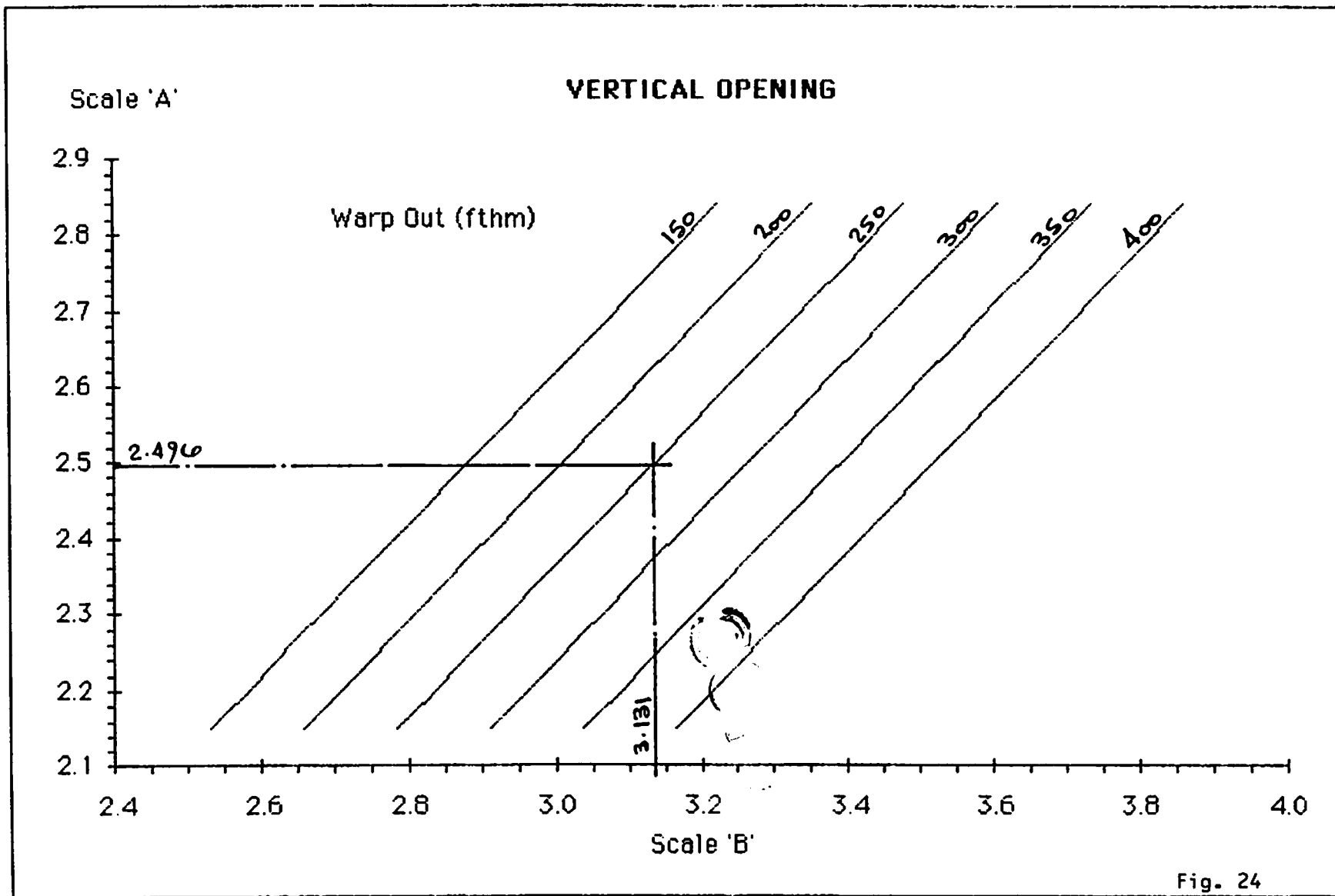
Scale 'B'



Vessel Distance Apart (nm)

Scale 'C'

Fig. 23



# VERTICAL OPENING

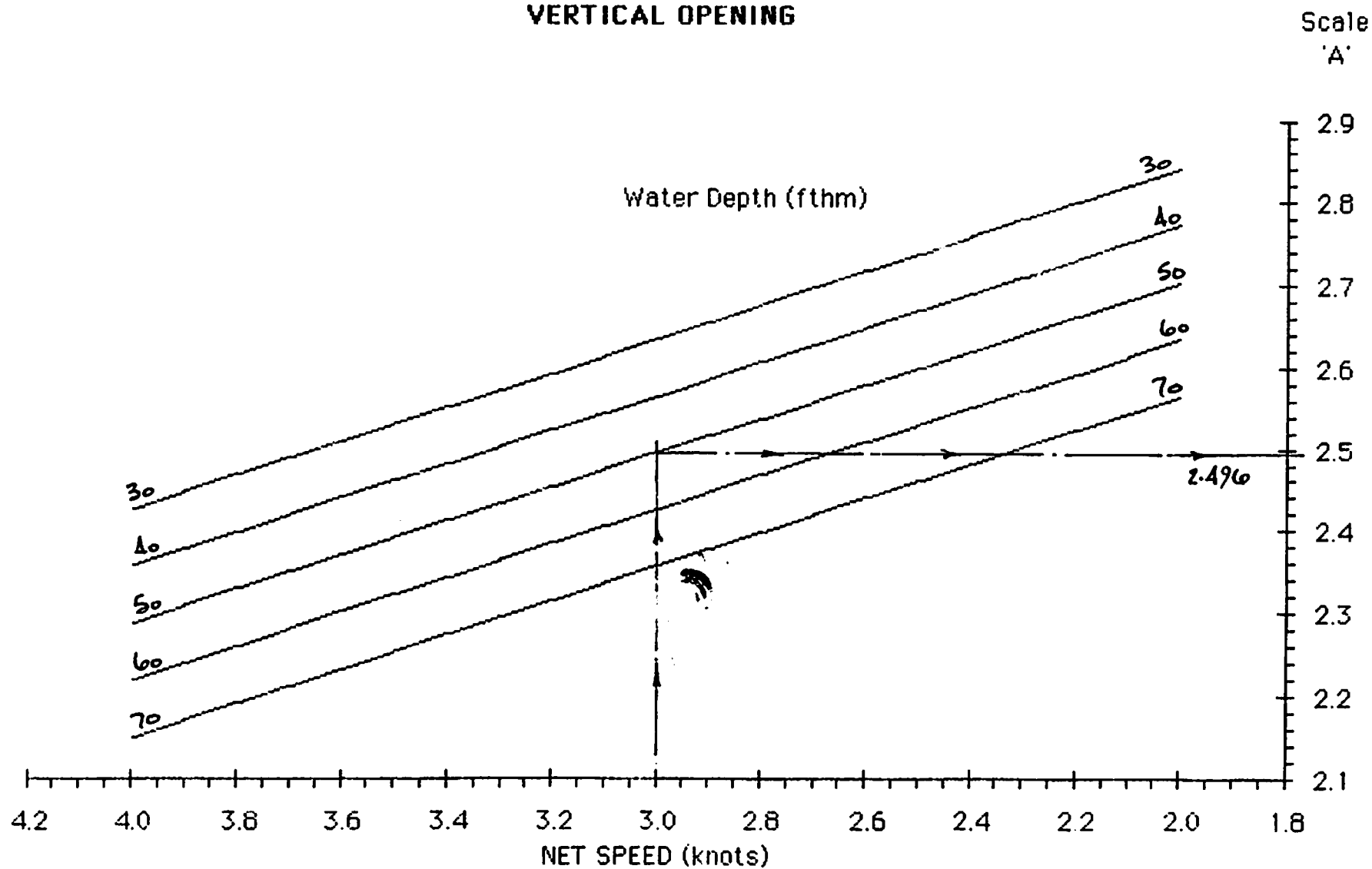


Fig. 25

VERTICAL OPENING

Scale 'C'

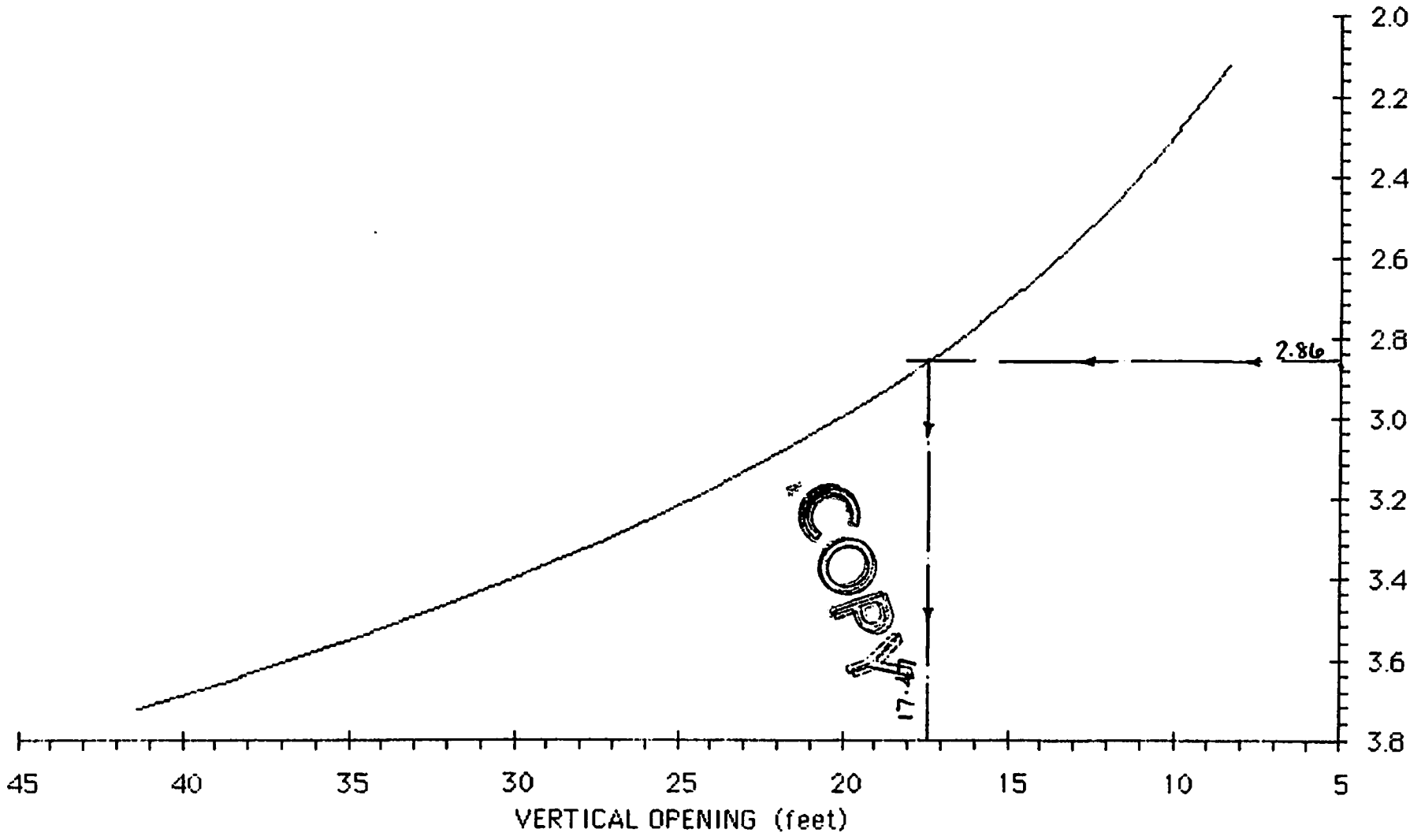


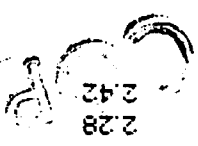
Fig. 26

ANALYSED VALUES FOR AVERAGE TOW PARAMETERS ON TRIAL

TABLE 1

Values of WT, Ho, Vo @ Net Speeds(Vn) for each Warp Length(W) & Vessel Distance(D)

Distance=		0.15 n.m.	
Warp Length=	175 fthm	250 fthm	
Ave mean d=	21 fthm	51.75 fthm	
Net Speed	VS (knots)	VS (knots)	VS (knots)
Warp Tension	WT (tons)	WT (tons)	WT (tons)
Hor. Opng.	Ho (ft)	Ho (ft)	Ho (ft)
Vert. Opng.	Vo (ft)	Vo (ft)	Vo (ft)
2.4	1.74	1.59	1.59
2.6	1.84	1.69	1.69
2.8	1.96	1.79	1.79
3.0	2.08	1.90	1.90
3.2	2.21	2.02	2.02
3.4	2.35	2.14	2.14
3.6	2.49	2.28	2.28
3.8	2.64	2.42	2.42
2.4	92.43	21.39	21.39
2.6	92.00	20.52	20.52
2.8	91.58	19.69	19.69
3.0	91.16	18.88	18.88
3.2	90.74	18.12	18.12
3.4	90.32	17.38	17.38
3.6	89.91	16.67	16.67
3.8	89.50	15.99	15.99
Warp Length=	300 fthm	350 fthm	
Ave mean d=	50.5 fthm(assumed)	57.5 fthm	
Net Speed	VS (knots)	VS (knots)	VS (knots)
Warp Tension	WT (tons)	WT (tons)	WT (tons)
Hor. Opng.	Ho (ft)	Ho (ft)	Ho (ft)
Vert. Opng.	Vo (ft)	Vo (ft)	Vo (ft)
2.4	1.62	1.60	1.60
2.6	1.72	1.70	1.70
2.8	1.82	1.80	1.80
3.0	1.93	1.91	1.91
3.2	2.05	2.03	2.03
3.4	2.18	2.16	2.16
3.6	2.32	2.29	2.29
3.8	2.46	2.43	2.43
2.4	84.42	23.95	23.95
2.6	84.03	22.98	22.98
2.8	83.64	22.04	22.04
3.0	83.26	21.15	21.15
3.2	82.88	20.29	20.29
3.4	82.50	19.46	19.46
3.6	82.12	18.67	18.67
3.8	81.74	17.91	17.91
2.4	81.97	2.4	2.4
2.6	81.59	2.6	2.6
2.8	81.22	2.8	2.8
3.0	80.85	3.0	3.0
3.2	80.47	3.2	3.2
3.4	80.10	3.4	3.4
3.6	79.74	3.6	3.6
3.8	79.37	3.8	3.8
2.4	25.91	81.97	81.97
2.6	24.86	81.59	81.59
2.8	23.84	81.22	81.22
3.0	22.87	80.85	80.85
3.2	21.94	80.47	80.47
3.4	21.05	80.10	80.10
3.6	20.19	79.74	79.74
3.8	19.37	79.37	79.37



ANALYSED VALUES FOR AVERAGE TOW PARAMETERS ON TRIAL

TABLE 2

Values of WT, Ho, Vo @ Net Speeds(Vn) for each Warp Length(W) & Vessel Distance(D)

Distance= 0.20 n.m.				Warp Length= 250 fthm			
Warp Length= 175 fthm				Warp Length= 250 fthm			
Ave mean d= 17.67 fthm				Ave mean d= 51.08 fthm			
Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)	Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.86	100.92	20.46	2.4	1.68	93.47	19.64
2.6	1.97	100.46	19.63	2.6	1.78	93.04	18.84
2.8	2.09	100.00	18.83	2.8	1.90	92.62	18.07
3.0	2.22	99.54	18.06	3.0	2.01	92.19	17.34
3.2	2.36	99.08	17.33	3.2	2.14	91.77	16.63
3.4	2.51	98.63	16.62	3.4	2.27	91.35	15.96
3.6	2.66	98.17	15.94	3.6	2.41	90.93	15.31
3.8	2.83	97.72	15.30	3.8	2.56	90.51	14.69
Warp Length= 300 fthm				Warp Length= 350 fthm			
Ave mean d= 50.75 fthm(assumed)				Ave mean d= 51.67 fthm			
Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)	Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.71	91.71	22.35	2.4	1.72	89.82	25.22
2.6	1.81	91.29	21.44	2.6	1.83	89.41	24.19
2.8	1.92	90.87	20.57	2.8	1.94	89.00	23.20
3.0	2.04	90.45	19.73	3.0	2.06	88.59	22.26
3.2	2.17	90.04	18.93	3.2	2.19	88.18	21.35
3.4	2.30	89.62	18.16	3.4	2.33	87.78	20.48
3.6	2.45	89.21	17.42	3.6	2.47	87.37	19.65
3.8	2.60	88.80	16.71	3.8	2.62	86.97	18.85

ANALYSED VALUES FOR AVERAGE TOW PARAMETERS ON TRIAL

TABLE 3

Values of WT; Ho; Vo @ Net Speeds(Vn) for each Warp Length(W) & Vessel Distance(D)

Distance= 0.25 n.m

Warp Length= 175 fthm

Ave mean d= 17.25 fthm

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.97	109.75	19.18
2.6	2.09	109.24	18.40
2.8	2.22	108.74	17.65
3.0	2.35	108.24	16.93
3.2	2.50	107.74	16.24
3.4	2.65	107.25	15.58
3.6	2.82	106.75	14.95
3.8	2.99	106.26	14.34

Warp Length= 250 fthm

Ave mean d= 51.25 fthm

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.77	101.56	18.34
2.6	1.88	101.09	17.59
2.8	2.00	100.63	16.87
3.0	2.13	100.16	16.19
3.2	2.26	99.70	15.53
3.4	2.40	99.25	14.91
3.6	2.54	98.79	14.29
3.8	2.70	98.34	13.71

Warp Length= 300 fthm

Ave mean d= 50.5 fthm(assumed)

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.80	99.70	20.93
2.6	1.92	99.24	20.07
2.8	2.03	98.79	19.26
3.0	2.16	98.34	18.47
3.2	2.29	97.88	17.72
3.4	2.44	97.43	17.00
3.6	2.59	96.99	16.31
3.8	2.75	96.54	15.64

Warp Length= 350 fthm

Ave mean d= 56.5 fthm

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.79	96.95	22.79
2.6	1.90	96.50	21.87
2.8	2.02	96.06	20.98
3.0	2.14	95.62	20.12
3.2	2.27	95.18	19.30
3.4	2.42	94.74	18.52
3.6	2.57	94.31	17.76
3.8	2.72	93.87	17.04

PREDICTING VALUES FOR A CONSTANT WATER DEPTH

TABLE 4

Values of WT, Ho, Vo @ Net Speeds(Vn) for each Warp Length(W) & Vessel Distance(D)

Distance= 0.15 n.m.				Warp Length= 250 fthm			
Warp Length= 175 fthm				Warp Length= 250 fthm			
Ave mean d= 30 fthm				Ave mean d= 30 fthm			
Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)	Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.68	91.25	20.10	2.4	1.72	89.62	24.32
2.6	1.79	90.84	19.28	2.6	1.82	88.22	23.33
2.8	1.90	90.42	18.50	2.8	1.94	87.81	22.38
3.0	2.01	90.00	17.74	3.0	2.05	87.41	21.47
3.2	2.14	89.59	17.02	3.2	2.18	87.01	20.59
3.4	2.27	89.18	16.33	3.4	2.32	86.61	19.75
3.6	2.41	88.77	15.66	3.6	2.46	86.21	18.95
3.8	2.56	88.36	15.03	3.8	2.61	85.81	18.18

Warp Length= 300 fthm				Warp Length= 350 fthm			
Ave mean d= 30 fthm(assumed)				Ave mean d= 30 fthm			
Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)	Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Cong. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.74	86.91	27.61	2.4	1.76	85.23	31.35
2.6	1.85	86.51	26.49	2.6	1.87	84.84	30.07
2.8	1.96	86.12	25.41	2.8	1.99	84.45	28.85
3.0	2.08	85.72	24.37	3.0	2.11	84.06	27.67
3.2	2.21	85.33	23.38	3.2	2.24	83.68	26.55
3.4	2.35	84.93	22.43	3.4	2.38	83.29	25.47
3.6	2.49	84.54	21.52	3.6	2.53	82.91	24.43
3.8	2.65	84.16	20.64	3.8	2.68	82.53	23.44



PREDICTING VALUES FOR A CONSTANT WATER DEPTH

TABLE 5

Values of WT; Ho, Vo @ Net Speeds(Vn) for each Warp Length(W) & Vessel Distance(D)

Distance= 0.15 n.m.

Warp Length= 175 fthm

Warp Length= 250 fthm

Ave mean d= 50 fthm

Ave mean d= 50 fthm

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)	Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.56	88.70	17.50	2.4	1.60	86.14	21.17
2.6	1.68	88.29	16.79	2.6	1.70	85.75	20.31
2.8	1.76	87.89	16.10	2.8	1.80	85.35	19.48
3.0	1.87	87.48	15.45	3.0	1.91	84.96	18.69
3.2	1.99	87.08	14.82	3.2	2.03	84.57	17.93
3.4	2.11	86.68	14.22	3.4	2.16	84.18	17.20
3.6	2.24	86.28	13.64	3.6	2.29	83.80	16.50
3.8	2.38	85.89	13.08	3.8	2.43	83.41	15.83

Warp Length= 300 fthm

Warp Length= 350 fthm

Ave mean d= 50 fthm(assumed)

Ave mean d= 50 fthm

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)	Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.62	84.48	24.04	2.4	1.64	82.85	27.28
2.6	1.72	84.09	23.06	2.6	1.74	82.47	26.18
2.8	1.83	83.70	22.12	2.8	1.85	82.09	25.12
3.0	1.94	83.32	21.22	3.0	1.96	81.71	24.09
3.2	2.06	82.94	20.36	3.2	2.09	81.34	23.11
3.4	2.19	82.56	19.53	3.4	2.22	80.96	22.17
3.6	2.32	82.18	18.73	3.6	2.35	80.59	21.27
3.8	2.46	81.80	17.97	3.8	2.50	80.22	20.40

PREDICTING VALUES FOR A CONSTANT WATER DEPTH

TABLE 6

Values of WT; Ho; Vo @ Net Speeds(Vn) for each Warp Length(W) & Vessel Distance(D)

Distance= 0.15 n.m.

Warp Length= 175 fthm

Ave mean d= 70 fthm

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.46	86.22	15.24
2.6	1.55	85.82	14.61
2.8	1.64	85.43	14.02
3.0	1.74	85.03	13.45
3.2	1.85	84.64	12.90
3.4	1.97	84.25	12.38
3.6	2.09	83.87	11.87
3.8	2.22	83.48	11.39

Warp Length= 250 fthm

Ave mean d= 70 fthm

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.49	83.73	15.43
2.6	1.58	83.35	14.68
2.8	1.68	82.96	13.96
3.0	1.78	82.58	13.27
3.2	1.89	82.20	12.61
3.4	2.01	81.82	11.97
3.6	2.13	81.45	11.36
3.8	2.26	81.07	10.78

Warp Length= 300 fthm

Ave mean d= 70 fthm(assumed)

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.51	82.11	20.93
2.6	1.60	81.74	20.08
2.8	1.70	81.36	19.26
3.0	1.80	80.99	18.48
3.2	1.92	80.61	17.72
3.4	2.03	80.24	17.00
3.6	2.16	79.88	16.31
3.8	2.29	79.51	15.65

Warp Length= 350 fthm

Ave mean d= 70 fthm

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.53	80.53	23.76
2.6	1.62	80.16	22.80
2.8	1.72	79.79	21.87
3.0	1.83	79.42	20.96
3.2	1.94	79.06	20.12
3.4	2.06	78.69	19.30
3.6	2.19	78.33	18.52
3.8	2.32	77.97	17.76

PREDICTING VALUES FOR A CONSTANT WATER DEPTH

TABLE 7

Values of WT; Ho; Vo @ Net Speeds(Vn) for each Warp Length(W) & Vessel Distance(D)

Distance= 0.2 n.m

Warp Length= 175 fthm

Ave mean d= 30 fthm

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.78	99.17	18.79
2.6	1.89	98.72	18.02
2.8	2.00	98.26	17.29
3.0	2.13	97.81	16.58
3.2	2.26	97.36	15.91
3.4	2.40	96.91	15.26
3.6	2.55	96.47	14.64
3.8	2.71	96.03	14.04

Warp Length= 250 fthm

Ave mean d= 30 fthm

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.93	96.31	22.73
2.6	2.03	95.87	21.90
2.8	2.14	95.43	20.91
3.0	2.17	94.99	20.06
3.2	2.31	94.56	19.25
3.4	2.45	94.12	18.46
3.6	2.60	93.69	17.71
3.8	2.76	93.26	16.99

Warp Length= 300 fthm

Ave mean d= 30 fthm(assumed)

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.84	94.45	25.80
2.6	1.95	94.02	24.75
2.8	2.07	93.59	23.75
3.0	2.20	93.16	22.78
3.2	2.34	92.73	21.85
3.4	2.48	92.30	20.96
3.6	2.64	91.88	20.11
3.8	2.80	91.46	19.29

Warp Length= 350 fthm

Ave mean d= 30 fthm

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.86	92.63	29.30
2.6	1.98	92.20	28.11
2.8	2.10	91.78	26.96
3.0	2.23	91.36	25.87
3.2	2.37	90.94	24.81
3.4	2.52	90.52	23.80
3.6	2.67	90.11	22.83
3.8	2.84	89.69	21.90

PREDICTING VALUES FOR A CONSTANT WATER DEPTH

TABLE 8

Values of WT, Ho, Vo @ Net Speeds(Vn) for each Warp Length(W) & Vessel Distance(D)

Distance= 0.2 n.m.

Warp Length= 175 fthm

Ave mean d= 50 fthm

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.65	96.39	16.36
2.6	1.76	95.95	15.69
2.8	1.86	95.51	15.05
3.0	1.98	95.07	14.44
3.2	2.10	94.64	13.85
3.4	2.23	94.20	13.29
3.6	2.37	93.77	12.75
3.8	2.52	93.34	12.23

Warp Length= 250 fthm

Ave mean d= 50 fthm

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.69	93.62	19.79
2.6	1.79	93.19	18.98
2.8	1.90	92.76	18.21
3.0	2.02	92.33	17.47
3.2	2.15	91.91	16.76
3.4	2.28	91.49	16.07
3.6	2.42	91.07	15.42
3.8	2.57	90.65	14.79

Warp Length= 300 fthm

Ave mean d= 50 fthm(assumed)

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.71	91.81	22.47
2.6	1.82	91.39	21.55
2.8	1.93	90.97	20.68
3.0	2.05	90.55	19.83
3.2	2.17	90.13	19.03
3.4	2.31	89.72	18.25
3.6	2.45	89.31	17.51
3.8	2.60	88.90	16.80

Warp Length= 350 fthm

Ave mean d= 50 fthm

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.73	90.04	25.51
2.6	1.84	89.62	24.47
2.8	1.95	89.21	23.47
3.0	2.08	88.80	22.52
3.2	2.20	88.39	21.60
3.4	2.34	87.99	20.72
3.6	2.49	87.58	19.88
3.8	2.64	87.18	19.07

COPY

PREDICTING VALUES FOR A CONSTANT WATER DEPTH

TABLE 9

Values of WT; Ho, Vo @ Net Speeds(Vn) for each Warp Length(W) & Vessel Distance(D)

Distance= 0.2 n.m.

Warp Length= 175 fthm

Warp Length= 250 fthm

Ave mean d= 70 fthm

Ave mean d= 70 fthm

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)	Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.54	93.70	14.24	2.4	1.57	90.99	17.23
2.6	1.63	93.27	13.66	2.6	1.67	90.58	16.53
2.8	1.73	92.84	13.10	2.8	1.77	90.16	15.85
3.0	1.84	92.41	12.57	3.0	1.88	89.75	15.21
3.2	1.96	91.99	12.06	3.2	2.00	89.33	14.59
3.4	2.08	91.56	11.57	3.4	2.12	88.92	14.00
3.6	2.21	91.14	11.10	3.6	2.25	88.52	13.43
3.8	2.34	90.72	10.65	3.8	2.39	88.11	12.89

COPY

Warp Length= 300 fthm

Warp Length= 350 fthm

Ave mean d= 70 fthm(assumed)

Ave mean d= 70 fthm

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)	Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.59	89.24	19.56	2.4	1.61	87.51	22.21
2.6	1.69	88.83	18.76	2.6	1.71	87.11	21.31
2.8	1.79	88.42	18.00	2.8	1.82	86.71	20.44
3.0	1.91	88.01	17.27	3.0	1.93	86.31	19.61
3.2	2.02	87.61	16.57	3.2	2.05	85.92	18.81
3.4	2.15	87.21	15.89	3.4	2.18	85.52	18.04
3.6	2.28	86.81	15.24	3.6	2.31	85.13	17.31
3.8	2.42	86.41	14.62	3.8	2.46	84.74	16.60

PREDICTING VALUES FOR A CONSTANT WATER DEPTH

TABLE 10

Values of WT, Ho, Vo @ Net Speeds(Vn) for each Warp Length(W) & Vessel Distance(D)

Distance= 0.25 n.m.				Warp Length= 250 fthm			
Warp Length= 175 fthm				Ave mean d= 30 fthm			
Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)	Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.88	107.78	17.56	2.4	1.92	104.67	21.24
2.6	1.99	107.28	16.84	2.6	2.03	104.19	20.38
2.8	2.12	106.79	16.16	2.8	2.16	103.71	19.55
3.0	2.25	106.30	15.50	3.0	2.29	103.23	18.75
3.2	2.39	105.81	14.87	3.2	2.44	102.76	17.99
3.4	2.53	105.32	14.26	3.4	2.59	102.29	17.26
3.6	2.69	104.84	13.68	3.6	2.75	101.82	16.55
3.8	2.86	104.36	13.13	3.8	2.92	101.35	15.86

Warp Length= 300 fthm				Warp Length= 350 fthm			
Ave mean d= 30 fthm(assumed)				Ave mean d= 30 fthm			
Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)	Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.94	102.65	24.12	2.4	1.97	100.67	27.38
2.6	2.06	102.18	23.14	2.6	2.09	100.20	26.27
2.8	2.19	101.71	22.20	2.8	2.22	99.74	25.19
3.0	2.33	101.24	21.29	3.0	2.36	99.28	24.16
3.2	2.47	100.77	20.43	3.2	2.50	98.83	23.19
3.4	2.62	100.31	19.59	3.4	2.66	98.37	22.25
3.6	2.78	99.85	18.80	3.6	2.82	97.92	21.34
3.8	2.96	99.39	18.03	3.8	3.00	97.47	20.47

PREDICTING VALUES FOR A CONSTANT WATER DEPTH

TABLE 11

Values of WT; Ho; Vo @ Net Speeds(Vn) for each Warp Length(W) & Vessel Distance(D)

Distance= 0.25 n.m.				Warp Length= 250 fthm			
Warp Length= 175 fthm				Warp Length= 250 fthm			
Ave mean d= 50 fthm				Ave mean d= 50 fthm			
Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)	Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.75	104.76	15.29	2.4	1.78	101.74	18.49
2.6	1.96	104.28	14.66	2.6	1.89	101.27	17.74
2.8	1.97	103.80	14.07	2.8	2.01	100.81	17.02
3.0	2.09	103.32	13.49	3.0	2.13	100.34	16.33
3.2	2.22	102.85	12.95	3.2	2.27	99.88	15.66
3.4	2.36	102.37	12.42	3.4	2.41	99.42	15.02
3.6	2.50	101.90	11.91	3.6	2.56	98.97	14.41
3.8	2.66	101.44	11.43	3.8	2.71	98.51	13.83

Warp Length= 300 fthm				Warp Length= 350 fthm			
Ave mean d= 50 fthm(assumed)				Ave mean d= 50 fthm			
Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)	Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.81	99.77	21.00	2.4	1.83	97.85	23.84
2.6	1.92	99.32	20.14	2.6	1.94	97.40	22.87
2.8	2.04	98.86	19.32	2.8	2.07	96.95	21.94
3.0	2.16	98.41	18.54	3.0	2.19	96.50	21.05
3.2	2.30	97.95	17.78	3.2	2.33	96.06	20.19
3.4	2.44	97.50	17.06	3.4	2.47	95.62	19.37
3.6	2.59	97.06	16.36	3.6	2.63	95.18	18.58
3.8	2.75	96.61	15.70	3.8	2.79	94.74	17.82

PREDICTING VALUES FOR A CONSTANT WATER DEPTH

TABLE 12

Values of WT, Ho, Vo @ Net Speeds(Vn) for each Warp Length(W) & Vessel Distance(D)

Distance= 0.25 n.m.

Warp Length= 175 fthm

Ave mean d= 70 fthm

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.65	101.82	13.31
2.6	1.73	101.36	12.77
2.8	1.83	100.89	12.25
3.0	1.95	100.43	11.75
3.2	2.07	99.97	11.27
3.4	2.19	99.51	10.81
3.6	2.33	99.05	10.37
3.8	2.48	98.60	9.95

Warp Length= 250 fthm

Ave mean d= 70 fthm

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.66	98.89	16.10
2.6	1.76	98.44	15.45
2.8	1.87	97.98	14.82
3.0	1.99	97.53	14.21
3.2	2.11	97.09	13.64
3.4	2.24	96.64	13.09
3.6	2.38	96.20	12.55
3.8	2.53	95.75	12.04

Warp Length= 300 fthm

Ave mean d= 70 fthm (assumed)

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.68	96.98	18.28
2.6	1.79	96.53	17.54
2.8	1.90	96.09	16.82
3.0	2.01	95.65	16.14
3.2	2.14	95.21	15.48
3.4	2.27	94.77	14.85
3.6	2.41	94.34	14.25
3.8	2.56	93.90	13.67

Warp Length= 350 fthm

Ave mean d= 70 fthm

Net Speed Vs (knots)	Warp Tension WT (tons)	Hor. Opng. Ho (ft)	Vert. Opng. Vo (Ft)
2.4	1.70	95.11	20.76
2.6	1.81	94.67	19.91
2.8	1.92	94.24	19.10
3.0	2.04	93.80	18.33
3.2	2.17	93.37	17.59
3.4	2.30	92.94	16.86
3.6	2.44	92.52	16.18
3.8	2.59	92.09	15.52



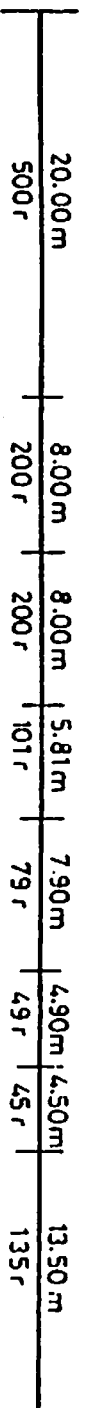
TABLE 13

EFFECT OF CHANGING ONE VARIABLE WHILST MAINTAINING THE VALUES  
OF THE REMAINING VARIABLES

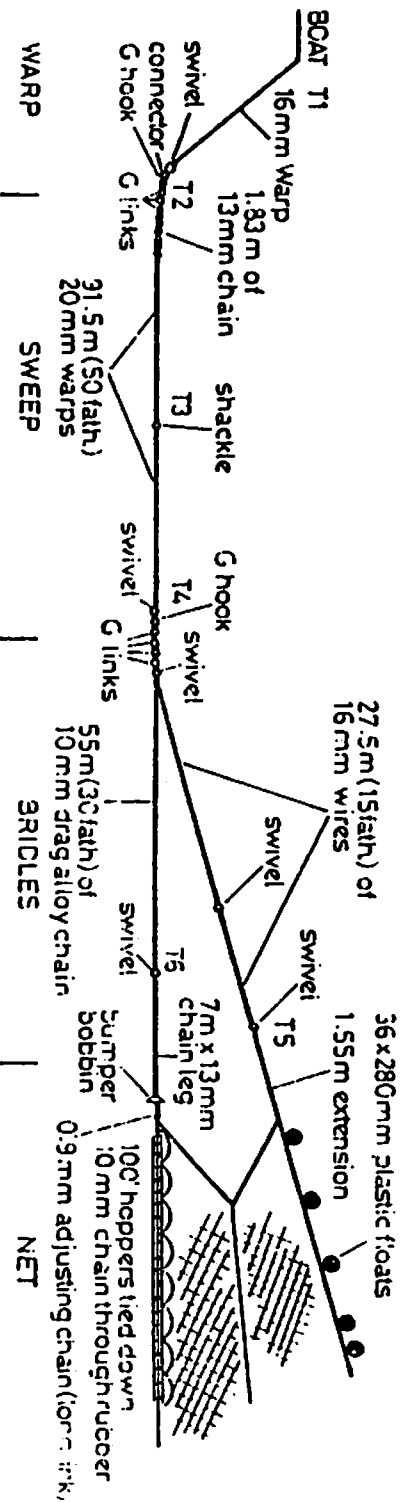
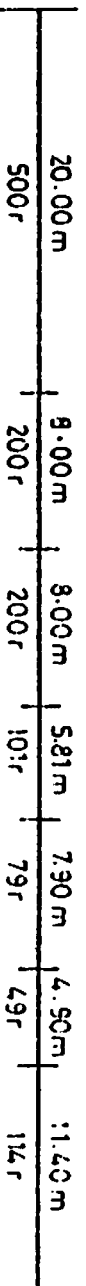
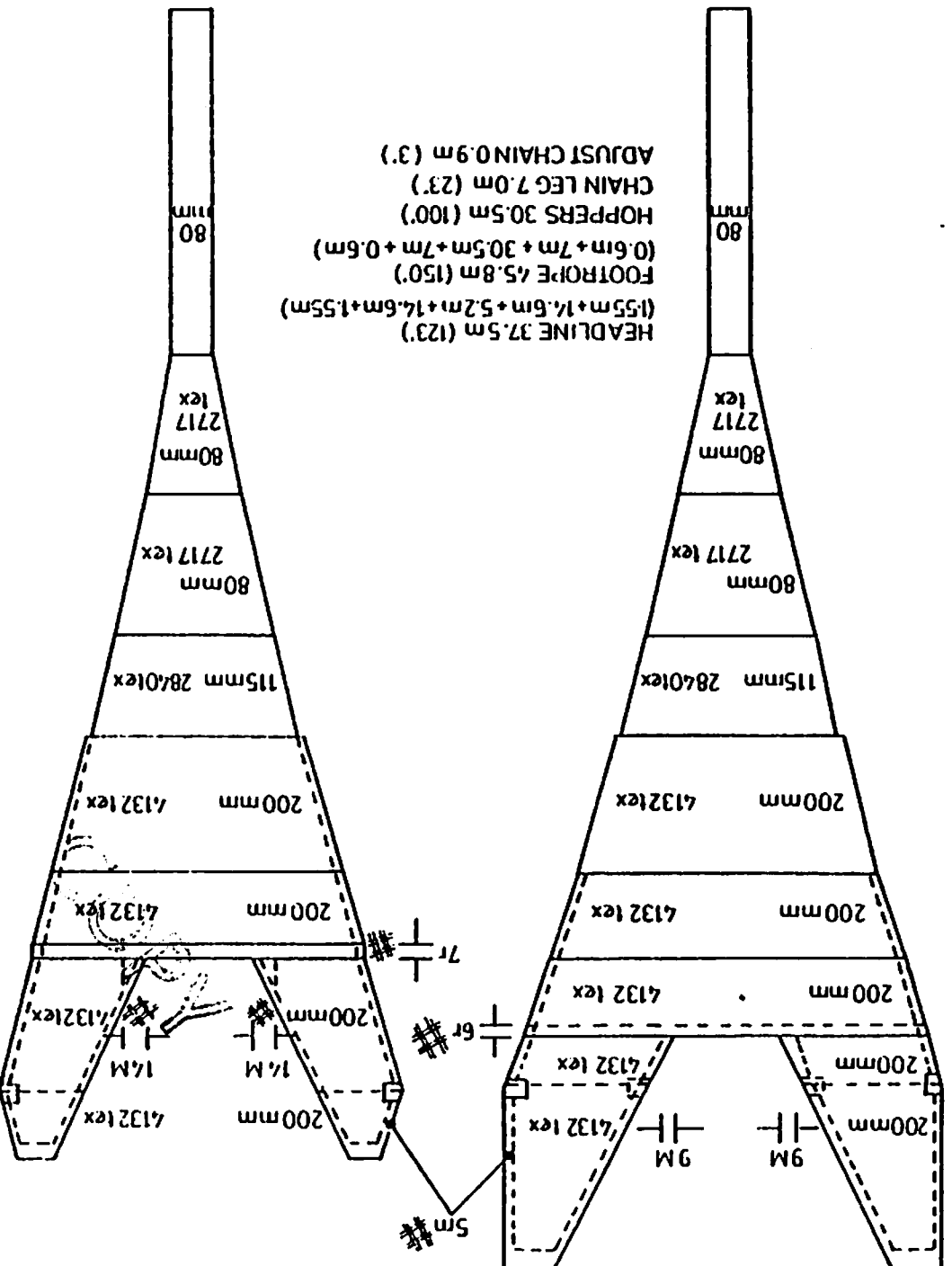
The effects are expressed as percentages of the original values

COPY

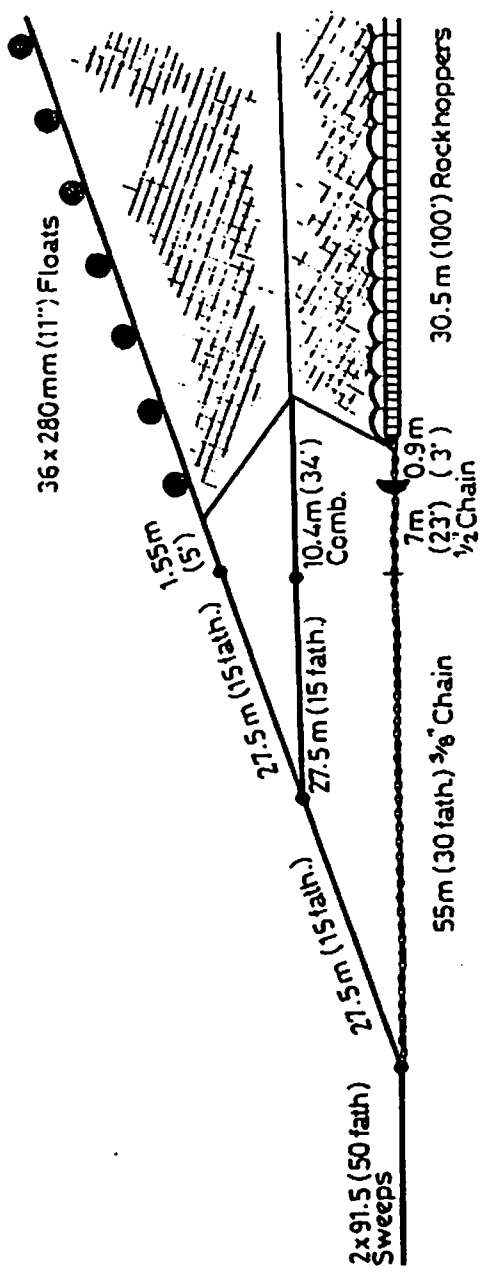
VARIABLE INCREASED	APPROX % CHANGE		
	WARP TENSION	HORIZONTAL OPENING	VERTICAL OPENING
SPEED per knot	+35	- 2	-19
WARP per 50 fathoms	+ 1.4	- 2	+13.5
DISTANCE per 1/10 naut mile	+11	+16.6	-13.5
WATER DEPTH per 10 fathoms	- 3.6	- 1.4	-10.9



HEADLINE 37.5 m (123')  
 (155m+14.6m+5.2m+14.6m+1.55m)  
 FOOTROPE 45.8 m (150')  
 (0.6m+7m+30.5m+7m+0.6m)  
 HOPPERS 30.5 m (100')  
 CHAIN LEG 7.0 m (23')  
 ADJUST CHAIN 0.9 m (3')

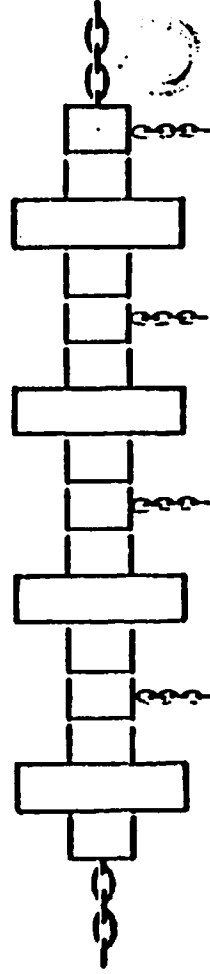


**F.M.A. Buckie Pair Trawl BT 154**  
(Rigged with two bridles and rockhopper gear)

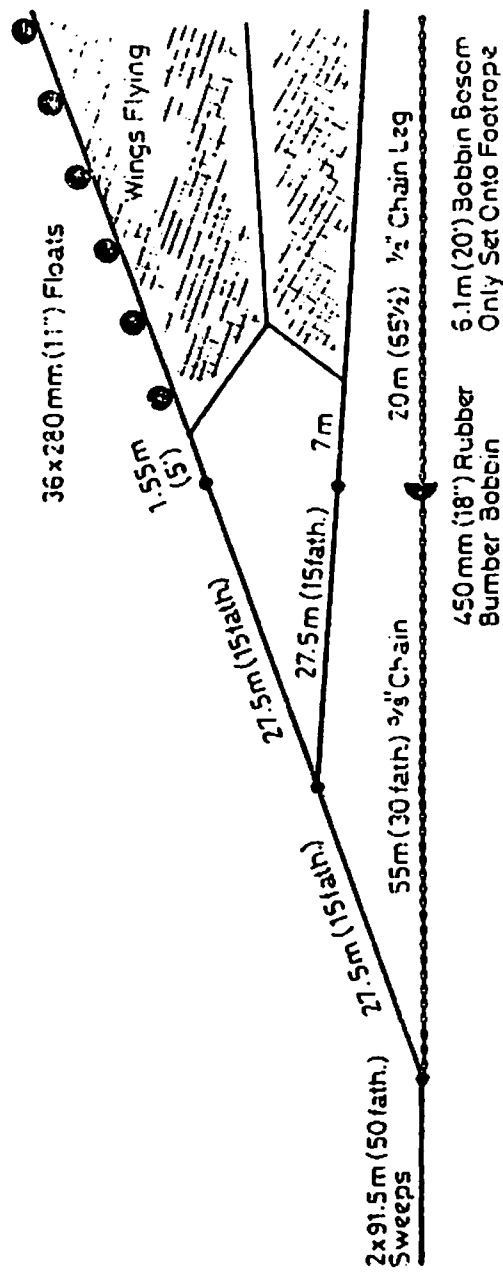


### 3 Bridle and Rockhopper Rig

3.05m (10')



Bobbins. 2 off x 10 ft. Strings Giving 20 ft. Bobbin Sosom



AVERAGE RESULTS OF RECORDED PARAMETERS DERIVED BY DAPS

TOW REF.    DAPS    AP04/4                    DATE 29TH FEBRUARY 1984  
                   SFJA            1/-  
 WARP OUT 175 FATHOMS    TRAWL RIG    2 BRIDLE WITH ROCKHOPPER GEAR

	1	2	3	4	5	6	7	8	9	10
BLOCK NO.										
Vessel Distance Apart (nm)	0.20	0.20	0.20	0.25	0.15	0.20	0.20	0.20	0.25	0.15
Engine RPM	1400	1500	1450	1450	1450	1400	1500	1450	1450	1450
<b>AQUILA</b>										
Warp Tension T1 starb (tons)	2.50	2.85	2.70	2.70	2.42	2.25	2.67	2.35	2.35	2.40
Ship Speed (knots)	2.90	3.15	3.00	3.20	3.30	2.55	2.65	3.10	3.10	2.95
Warp Declination (deg)	9	8	8.5	9.5	10	9.5	8	8	8.5	9
Water Depth (flm)	19	18	18	24	26	20	15	15	12	16
<b>POSEIDON</b>										
Warp Tension T1 port (tons)	2.07	2.35	2.24	2.12	1.93	1.90	1.95	1.80	2.10	1.93
Ship Speed (knots)	3.07	3.15	3.10	2.88	3.05	3.00	3.00	3.50	2.50	3.00
Warp Declination (deg)	-	-	-	-	-	-	-	-	-	-
Water Depth (flm)	17	14	14	18	24	24	20	18	15	18
<b>SPREADS (FEET)</b>										
Wing End	98	97	98	100	90	100	103	102	110	93
Mid Bridle	-	-	-	-	-	-	-	-	-	-
Fore Sweep	-	-	-	-	-	-	-	-	-	-
<b>TENSIONS (TONS)</b>										
T2 starb	-	-	-	-	-	-	-	-	-	-
T2 port	2.00	2.28	2.17	2.08	1.84	1.80	1.85	1.76	2.05	1.82
T3 starb	-	-	-	-	-	-	-	-	-	-
T3 port	-	-	-	-	-	-	-	-	-	-
T4 starb	-	-	-	-	-	-	-	-	-	-
T4 port	-	-	-	-	-	-	-	-	-	-
T5 starb	-	-	-	-	-	-	-	-	-	-
T5 port	0.98	1.05	1.02	1.03	0.90	0.87	0.94	0.84	1.02	0.77
T6 starb	0.81	0.95	0.95	0.90	0.83	0.80	0.95	0.80	0.80	0.84
T6 port	-	-	-	-	-	-	-	-	-	-
<b>VERTICAL OPENING (FEET)</b>										
Acoustic Meter	-	-	-	-	-	-	-	-	-	-
Manometer	18	17	17	17	19	20	19	19.5	18	20
NET SPEED (KNOTS)	3.05	3.35	3.20	2.95	3.10	2.70	2.80	2.60	2.65	2.75

APPENDIX III

AVERAGE RESULTS OF RECORDED PARAMETERS DERIVED BY DAFS

TOW REP.    DAFS    AP84/6                    DATE 1ST MARCH 1984  
                       SP1A            3/-  
 WARP OUT 250 FATHOMS    TRAWL RIG    2 BRIDLE WITH ROCKHOPPER GEAR

	1	2	3	4	5	6	7	8	9	10
BLOCK NO.										
Vessel Distance Apart (nm)	0.15	0.25	0.20	0.20	0.20	0.15	0.25	0.20	0.20	0.20
Engine RPM	1450	1450	1450	1550	1350	1450	1450	1450	1550	1350
<b>AQUILA</b>										
Warp Tension T1 starb (tons)	2.45	2.55	2.50	2.80	2.15	2.20	2.30	2.15	2.45	1.95
Ship Speed (knots)	3.15	3.10	3.00	3.50	3.10	3.15	2.90	3.80	3.90	3.30
Warp Declination (deg)	13	13	13	12.5	14	13.5	13	13	12.5	14
Water Depth (fthm)	55	54	50	51	56	52	48	47	49	47
<b>POSEIDON</b>										
Warp Tension T1 port (tons)	2.20	2.25	2.20	2.45	1.90	2.00	2.00	1.90	2.15	1.75
Ship Speed (knots)	2.95	2.95	3.30	3.45	3.05	3.30	3.50	3.70	4.00	3.30
Warp Declination (deg)	13.5	13.5	13	12.5	14.5	14.5	13.5	14.5	12.5	15.5
Water Depth (fthm)	46	47	45	49	52	54	50	53	56	58
<b>SPREADS (FEET)</b>										
Wing End	-	-	-	-	-	-	102	92	-	90
Mid Bridle	135	150	147	148	149	140	160	145	147	148
Fore Sweep	-	-	-	-	-	-	-	-	-	-
<b>TENSIONS (TONS)</b>										
T2 starb	2.44	2.54	2.46	2.72	2.08	2.12	2.28	2.04	2.34	1.84
T2 port	-	-	-	-	-	-	-	-	-	-
T3 starb	-	-	-	-	-	-	-	-	-	-
T3 port	-	-	-	-	-	-	-	-	-	-
T4 starb	2.70	2.54	2.40	2.73	2.02	2.10	2.26	2.00	2.36	1.77
T4 port	2.04	2.08	2.00	2.24	1.73	1.82	1.84	1.69	1.92	1.52
T5 starb	1.09	1.09	1.09	1.10	1.04	1.04	1.06	0.99	1.07	0.93
T5 port	1.06	1.08	1.04	1.10	0.90	0.90	0.94	0.85	0.98	0.82
T6 starb	0.84	0.90	0.86	0.89	0.73	0.78	0.84	0.74	0.87	0.66
T6 port	0.84	0.83	0.82	0.83	0.71	0.80	0.76	0.72	0.82	0.63
<b>VERTICAL OPENING (FEET)</b>										
Acoustic Meter	17	17	16	-	17	17	16	17	-	18
Manometer	-	-	-	-	-	-	-	-	-	-
<b>NET SPEED (KNOTS)</b>	<b>3.60</b>	<b>3.30</b>	<b>3.35</b>	<b>3.60</b>	<b>3.05</b>	<b>3.05</b>	<b>2.75</b>	<b>2.85</b>	<b>3.15</b>	<b>2.75</b>

AVERAGE RESULTS OF RECORDED PARAMETERS DERIVED BY DAFS

TOW REF.    DAFS    AF84/7    DATE 5TH MARCH 1984

             SF1A    7/-

WARP OUT 350 FATHOMS    TRAWL RIG    2 BRIDLE WITH ROCKHOPPER GEAR

	1	2	3	4	5	6	7
<b>BLOCK NO.</b>							
Vessel Distance Apart (nm)	0.15	0.25	0.20	0.20	0.20	0.15	0.25
Engine RPM	1450	1450	1450	1550	1350	1450	1450
<b>AQUILA</b>							
Warp Tension T1 starb (tons)	1.97	2.07	2.10	2.33	1.84	2.43	2.54
Ship Speed (knots)	3.90	3.73	3.64	4.30	3.40	3.20	2.84
Warp Declination (deg)	15	14.5	14	13	15.5	13.5	13
Water Depth (fthm)	57	56	51	49	52	56	51
<b>POSEIDON</b>							
Warp Tension T1 port (tons)	1.40	1.35	1.35	1.60	0.83	-	-
Ship Speed (knots)	3.75	3.34	3.63	4.00	3.20	2.84	-
Warp Declination (deg)	16	15.5	15	13.5	15.5	-	-
Water Depth (fthm)	58	57	52	51	55	54	47
<b>SPREADS (FEET)</b>							
Wing End	82	97	87	88	-	-	-
Mid Bridle	-	-	-	175	172	150	-
Fore Sweep	540	720	635	600	610	480	-
<b>TENSIONS (TONS)</b>							
T2 starb	1.89	1.95	1.98	2.22	1.72	2.43	-
T2 port	1.57	1.80	1.73	2.05	1.54	2.10	-
T3 starb	-	-	-	-	-	-	-
T3 port	-	-	-	-	-	-	-
T4 starb	-	-	-	-	-	-	-
T4 port	-	-	-	-	-	-	-
T5 starb	-	-	-	-	-	-	-
T5 port	0.63	0.73	0.69	0.91	0.62	0.35	-
T6 starb	0.70	0.74	0.72	0.82	0.64	0.84	-
T6 port	0.53	0.59	0.56	0.69	0.49	0.73	-
<b>VERTICAL OPENING (FEET)</b>							
Acoustic Meter	25	23	25	20	26	20	-
Manometer	-	-	-	-	-	-	-
<b>NET SPEED (KNOTS)</b>	2.75	2.50	2.65	3.10	2.35	-	-

AVERAGE RESULTS OF RECORDED PARAMETERS DERIVED BY DAPS

TOW REF. DATE AP84/B DATE 6TH MARCH 1984

SRIA 7/-

WARP OUT 300 FATHOMS TRAWL RIG 3 BRIDLE WITH ROCKHOPPER GEAR

BLOCK NO.	Vessel Distance Apart (nm)	Engine RPM	AQUILA	Warp Tension T1 starb (tons)	Ship Speed (knots)	Warp Declination (deg)	Water Depth (fthm)	POSIDON	Warp Tension T1 port (tons)	Ship Speed (knots)	Warp Declination (deg)	Water Depth (fthm)	SPREADS (FEET)	Wing End	Mid Bridle	Fore Sweep	TENSIONS (TONS)	T2 starb	T2 port	Centre starb	Centre port	T4 starb	T4 port	T5 starb	T5 port	T6 starb	T6 port	VERTICAL OPENING (FEET)	Acoustic Meter	Handometer	NET SPEED (KNOTS)
1	0.15	1450	2.55	2.87	14.5	17.0	47	2.08	2.75	17.0	47	75	140	140	470	2.33	2.33	2.17	0.57	0.49	0.30	2.06	0.80	0.72	0.615	32	-	-	3.22		
2	0.25	1450	2.50	2.76	14.7	-	48	-	-	-	48	100	160	160	720	2.38	2.38	2.22	0.33	0.30	0.30	2.06	0.93	0.93	0.75	24	-	-	2.98		
3	0.20	1450	2.55	2.75	14.5	-	55	2.20	2.85	-	48	90	150	150	590	2.34	2.34	2.13	0.45	0.395	0.395	2.04	0.8	0.78	0.695	28	-	-	3.02		
4	0.20	1550	-	-	15.0	12.5	48	2.55	3.00	12.5	48	85	150	150	575	2.66	2.66	2.46	0.56	0.485	0.485	2.34	0.95	0.93	0.79	33	-	-	3.37		
5	0.20	1350	2.20	2.40	15.0	13.5	42	2.13	2.40	13.5	42	90	155	155	620	2.03	2.03	1.99	0.295	0.31	0.31	1.82	0.72	0.75	0.605	28	-	-	2.62		
6	0.15	1450	2.23	3.65	16.0	17.5	58	1.78	3.08	17.5	58	80	130	130	480	2.02	2.02	1.83	0.45	0.435	0.435	1.78	0.71	0.66	0.545	33	-	-	2.92		
7	0.25	1450	2.27	3.50	15.7	12.0	58	1.98	3.43	12.0	58	105	160	160	740	2.11	2.11	1.98	0.225	0.25	0.25	1.76	0.85	0.91	0.66	26	-	-	2.82		
8	0.20	1450	2.25	3.70	15.5	10.5	53	1.67	3.45	10.5	53	90	155	155	600	2.07	2.07	1.93	0.36	0.39	0.39	1.86	0.77	0.75	0.61	30	-	-	2.96		
9	0.20	1550	2.25	-	14.5	12.0	50	2.30	4.00	12.0	50	85	150	150	550	2.37	2.37	2.19	0.49	0.47	0.47	2.11	0.84	0.90	0.695	27	-	-	3.25		
10	0.20	1350	-	-	-	14.5	55	1.92	3.43	14.5	55	90	150	150	570	1.82	1.78	1.78	0.265	0.305	0.305	1.71	0.72	0.72	0.53	29	-	-	2.62		

AVERAGE RESULTS OF RECORDED PARAMETERS DERIVED BY DAFS

TOW REF.      DAFS      AP84/9      DATE 6TH MARCH 1984  
                      SF1A      U/-  
 WARP OUT 300 FATHOMS      TRAWL RIG      2 BRIDLE WITH ROCKHOPPER GEAR

	1	2	3	4	5	6
BLOCK NO.						
Vessel Distance Apart (nm)	0.20	0.20	0.20	0.20	0.20	0.20
Engine RPM	1450	1550	1350	1450	1550	1350
<b>AQUILA</b>						
Warp Tension T1 starb (tons)	2.45	2.75	2.15	2.35	2.65	2.10
Ship Speed (knots)	3.00	3.45	2.90	3.45	3.05	3.10
Warp Declination (deg)	15.5	14	16	14	14	16.5
Water Depth (fthm)	55	51	52	46	50	50
<b>POSEIDON</b>						
Warp Tension T1 port (tons)	2.52	2.70	2.15	2.60	2.65	2.20
Ship Speed (knots)	2.90	3.35	3.0	3.80	3.95	3.40
Warp Declination (deg)	15	13	15	12.5	13	15.5
Water Depth (fthm)	48	47	50	49	54	57
<b>SPREADS (FEET)</b>						
Wing End	90	90	95	-	-	-
Mid Bridle	145	145	150	150	150	145
Fore Sweep	580	590	590	600	620	590
<b>TENSIONS (TONS)</b>						
T2 starb	2.26	2.52	1.96	2.14	2.44	1.88
T2 port	2.06	2.26	1.72	1.91	2.22	1.72
T3 starb	-	-	-	-	-	-
T3 port	-	-	-	-	-	-
T4 starb	-	-	-	-	-	-
T4 port	-	-	-	-	-	-
T5 starb	1.06	1.09	0.96	0.96	1.06	0.84
T5 port	1.07	1.16	0.89	0.96	1.08	0.82
T6 starb	0.80	0.39	0.68	0.36	0.97	0.74
T6 port	-	-	-	-	-	-
<b>VERTICAL OPENING (FEET)</b>						
Acoustic Meter	-	-	-	-	-	-
Manometer	-	-	-	-	-	-
<b>NET SPEED (KNOTS)</b>	<b>3.35</b>	<b>3.62</b>	<b>3.00</b>	<b>3.02</b>	<b>3.32</b>	<b>2.74</b>



AVERAGE RESULTS OF RECORDED PARAMETERS DERIVED BY DAPS

TOW REF.      DAPS      AP84/10      DATE 7TH MARCH 1984

SFIA      9/-

WARP OUT 300 FATHOMS      TRAWL RTG      BOBBIN GEAR

	1	2	3	4	5	6	7	8	9
<b>BLOCK NO.</b>									
Vessel Distance Apart (nm)	0.15	0.25	0.20	0.20	0.15	0.25	0.20	0.20	0.20
Engine RPM	1450	1450	1450	1550	1450	1450	1450	1550	1350
<b>AQUILA</b>									
Warp Tension T1 starb (tons)	2.40	2.35	2.40	2.80	2.20	2.35	-	2.55	1.95
Ship Speed (knots)	3.15	3.25	3.10	3.20	3.70	3.40	3.75	4.25	3.75
Warp Declination (deg)	13	13	13	12	14	13	12.5	12	14.5
Water Depth (fthm)	50	48.5	49.5	51	59	58	53.5	53	56.5
<b>POSEIDON</b>									
Warp Tension T1 port (tons)	2.84	2.95	3.05	3.40	2.88	2.94	2.63	-	2.62
Ship Speed (knots)	3.03	2.90	3.05	3.27	3.70	3.35	3.70	4.20	3.45
Warp Declination (deg)	14.5	14.5	15	13.5	15.5	15.5	14.5	14.5	16.5
Water Depth (fthm)	54	51	55	55	57	56	50	48	50
<b>SPREADS (FEET)</b>									
Wing End	70	95	-	85	-	-	-	-	-
Mid Bridle	130	174	156	153	137	181	158	158	158
Fore Sweep	320	545	470	475	600	680	640	645	650
<b>TENSIONS (TONS)</b>									
T2 starb	2.03	2.00	2.03	2.17	1.91	1.96	1.93	2.01	1.79
T2 port	-	-	-	-	-	-	-	-	-
Centre starb	0.46	0.47	0.49	0.56	0.43	0.47	0.42	0.52	0.39
Centre port	0.53	0.55	0.54	0.65	0.50	0.53	0.48	0.60	0.42
T4 starb	2.03	2.00	2.04	2.17	1.91	1.96	1.92	2.02	1.75
T4 port	2.12	2.10	2.10	2.30	1.98	2.07	2.02	2.16	1.88
T5 starb	1.12	1.10	1.11	1.27	1.01	1.03	0.99	1.08	0.77
T5 port	1.22	1.23	1.22	1.24	1.18	1.13	1.17	1.23	1.04
T6 starb	0.26	0.24	0.28	0.30	0.21	0.22	0.26	0.24	0.17
T6 port	-	-	-	-	-	-	-	-	-
<b>VERTICAL OPENING (FEET)</b>									
Acoustic Meter	23	20	21	21	28.5	22	22	23	24
Manometer	-	-	-	-	-	-	-	-	-
<b>NET SPEED (KNOTS)</b>	3.38	3.07	3.20	3.58	3.19	2.98	3.07	3.31	2.67

AVERAGE RESULTS OF RECORDED PARAMETERS DERIVED BY DAFS

TOW REF.    DAFS    AP84/10                    DATE 7TH MARCH 1984  
                      SFIA    10/-  
 WARP OUT 300 FATHOMS    TRAWL RIG            BOBBIN GEAR

	10	11	12	13	14
<b>BLOCK NO.</b>					
Vessel Distance Apart (nm)	0.15	0.25	0.20	0.20	0.20
Engine RPM	1450	1450	1450	1550	1350
<b>AQUILA</b>					
Warp Tension Tl port (tons)	2.50	2.50	2.50	2.75	2.20
Ship Speed (knots)	3.15	2.95	3.15	3.50	3.10
Warp Declination (deg)	14.5	14	14	13	14.5
Water Depth (fthm)	58	56	-	54	55.5
<b>POSEIDON</b>					
Warp Tension Tl stbd (tons)	3.17	3.16	3.16	3.43	3.07
Ship Speed (knots)	3.00	3.10	3.40	3.45	2.65
Warp Declination (deg)	15	15	16	13.5	15.5
Water Depth (fthm)	58	56	55	55	56
<b>SPREADS (FEET)</b>					
Wing End	-	-	-	-	-
Mid Bridle	135	164	150	142	153
Fore Sweep	480	690	600	570	580
<b>TENSIONS (TONS)</b>					
T2 starb	1.92	2.01	1.98	2.09	1.95
T2 port	-	-	-	-	-
Centre stbd	0.42	0.45	0.44	0.50	0.41
Centre port	0.55	0.58	0.58	0.66	0.44
T4 starb	1.90	1.99	1.96	2.09	1.93
T4 port	2.18	2.16	2.13	2.23	1.88
T5 starb	1.13	1.14	1.12	1.23	1.05
T5 port	1.22	1.22	1.22	1.24	1.03
T6 starb	0.23	0.25	0.25	0.26	0.18
T6 port	-	-	-	-	-
<b>VERTICAL OPENING (FEET)</b>					
Acoustic Meter	24	20.5	19	21	23
Manometer	-	-	-	-	-
<b>NET SPEED (KNOTS)</b>	3.31	3.18	3.21	3.60	3.00

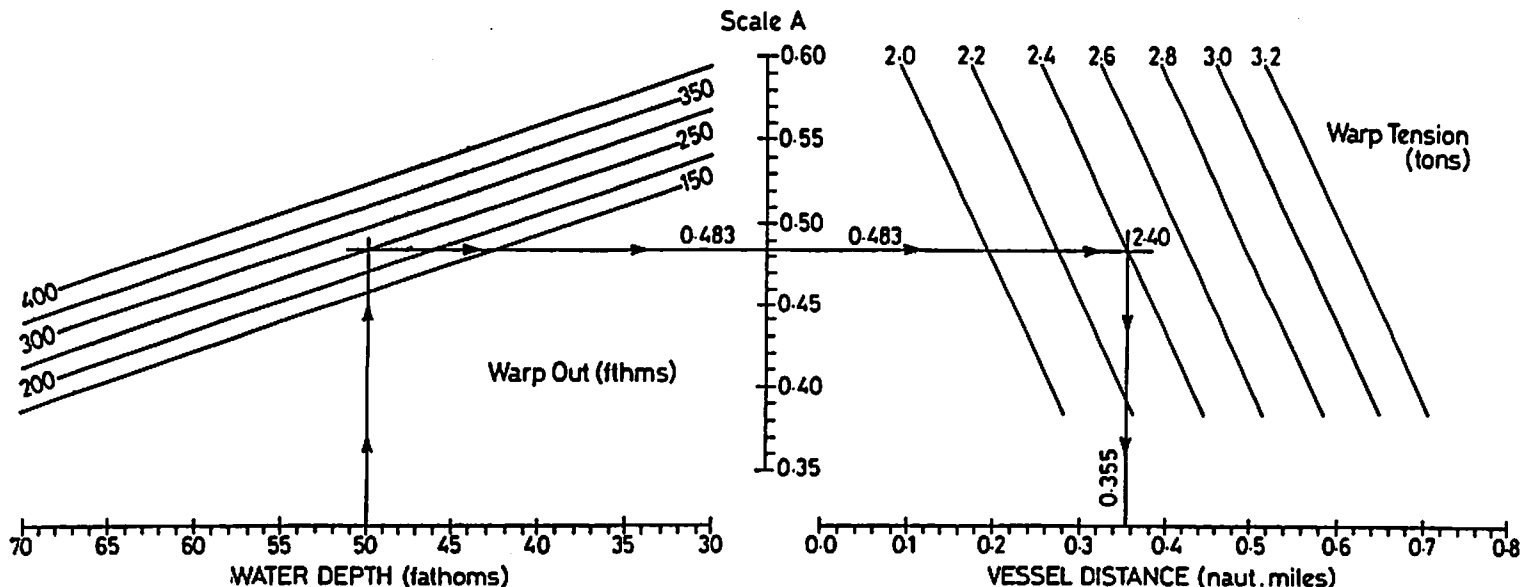
SUMMARY OF RECORDED DATA

WTd Denotes Warp Tension (tons) recorded by DAFS  
 WTa Denotes Warp Tension (knots) recorded by SFIA  
 Vn Denotes Net speed (knots)  
 d Denotes Water Depth (fathoms) - mean between vessels  
 Ho Denotes Horizontal Net Opening (feet)  
 Vo Denotes Vertical Net Opening (feet)  
 W Denotes Warp Out (fathoms)  
 D Denotes Vessel Distance Apart (naut. miles)

Tow Ref	AQUILA WTd	WTa	POSEIDON WTd	WTa	MEAN WT	Vs	D	Ho	Vo	W	d
1/1	2.50	2.10	2.07	2.26	2.23	3.05	0.20	98.00	18.00	175	18.0
2	2.65	2.47	2.35	2.48	2.23	3.35	0.20	97.00	17.00	175	18.0
3	2.70	2.33	2.24	2.33	2.23	3.20	0.20	98.00	17.00	175	16.1
4	2.70	2.22	2.12	2.58	2.23	2.95	0.25	108.00	17.00	175	21.1
5	2.42	2.00	1.93	2.07	2.23	3.10	0.15	90.00	19.00	175	29.0
6	2.25	1.76	1.90	2.07	2.23	2.70	0.20	100.00	20.00	175	22.0
7	2.67	2.11	1.95	2.07	2.23	2.80	0.20	103.00	19.00	175	17.5
8	2.35	1.79	1.80	2.05	2.23	2.60	0.20	102.00	19.50	175	16.5
9	2.35	1.75	2.10	2.32	2.23	2.65	0.25	110.00	18.00	175	18.5
10	2.40	1.73	1.93	2.24	2.23	2.75	0.15	83.00	20.00	175	17.0
<b>COPY</b>											
3/1	2.45	2.16	2.20	2.26	2.23	3.60	0.15		17	250	50.5
2	2.55	2.20	2.25	2.40	2.23	3.30	0.25		17	250	50.5
3	2.50	2.09	2.20	2.26	2.23	3.35	0.20		16	250	47.5
4	2.80	2.35	2.45	2.52	2.23	3.60	0.20			250	50.0
5	2.15	1.59	1.90	2.02	2.23	3.05	0.20		17	250	54.0
6	2.20	1.45	2.00	2.21	2.23	3.05	0.15		17	250	53.0
7	2.30	2.11	2.00	2.03	2.23	2.75	0.25	102.00	16	250	49.1
8	2.13	1.91	1.90	2.04	2.23	2.85	0.20	92.00	17	250	50.0
9	2.45	2.16	2.15	2.25	2.23	3.15	0.20			250	50.5
10	1.95	1.61	1.75	1.91	2.23	2.75	0.20	90.00	18	250	52.5
<b>COPY</b>											
6/1	1.97	2.06	1.40	1.62	2.23	2.75	0.15	82.00	25	350	57.5
2	2.07	2.13	1.35	1.53	2.23	2.50	0.25	87.00	23	350	56.5
3	2.10	2.11	1.35	1.75	2.23	2.65	0.20	87.00	25	350	51.5
4	2.33	2.33	1.60	2.04	2.23	3.10	0.20	88.00	20	350	50.0
5	1.84	1.80	0.83	3.09	2.23	2.35	0.20		26	350	53.5
6	2.43	2.51		2.19	2.23		0.15		20	350	57.0
7	2.54	2.67		2.52	2.23		0.25			350	49.0
<b>COPY</b>											
8/1	2.45	2.35	2.52	2.31	2.23	3.35	0.20	90.00		300	51.5
2	2.75	2.59	2.70	2.09	2.23	3.62	0.20	90.00		300	49.0
3	2.15	2.05	2.15	1.94	2.23	3.00	0.20	95.00		300	51.0
4	2.35	2.29	2.60	2.25	2.23	3.02	0.20			300	47.5
5	2.65	2.60	2.65	2.28	2.23	3.32	0.20			300	51.0
6	2.10	2.01	2.20	2.31	2.23	2.74	0.20			300	53.5

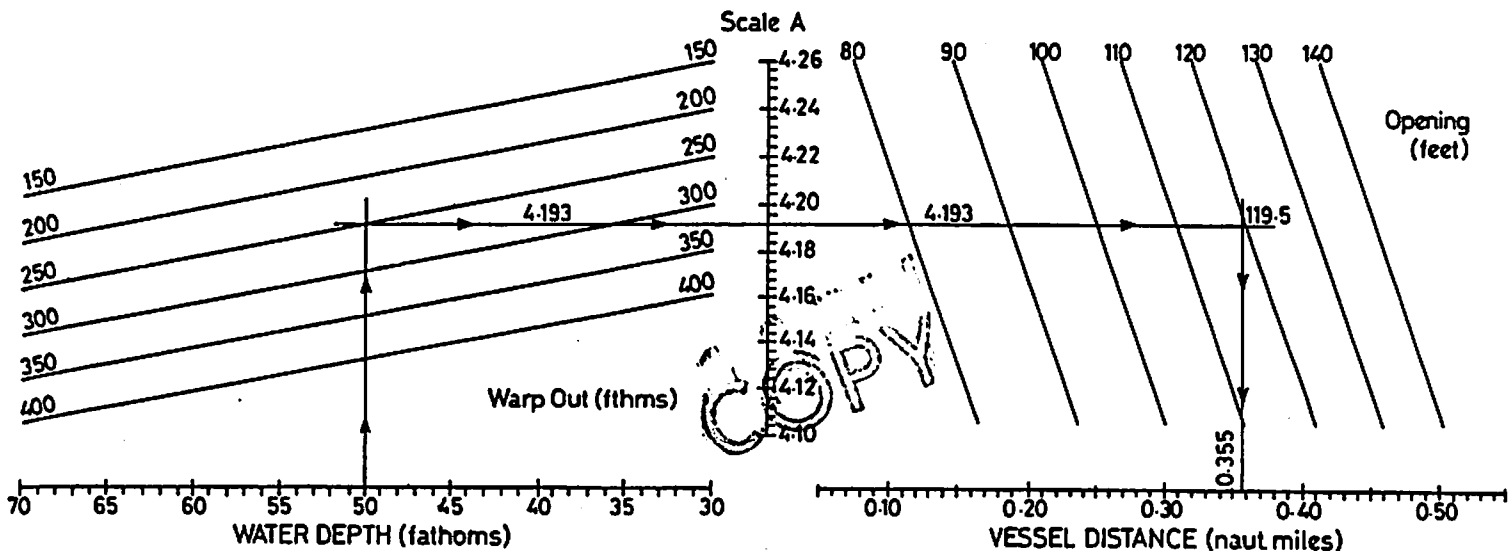
# SINGLE WARP TENSION

NET SPEED 3 knots



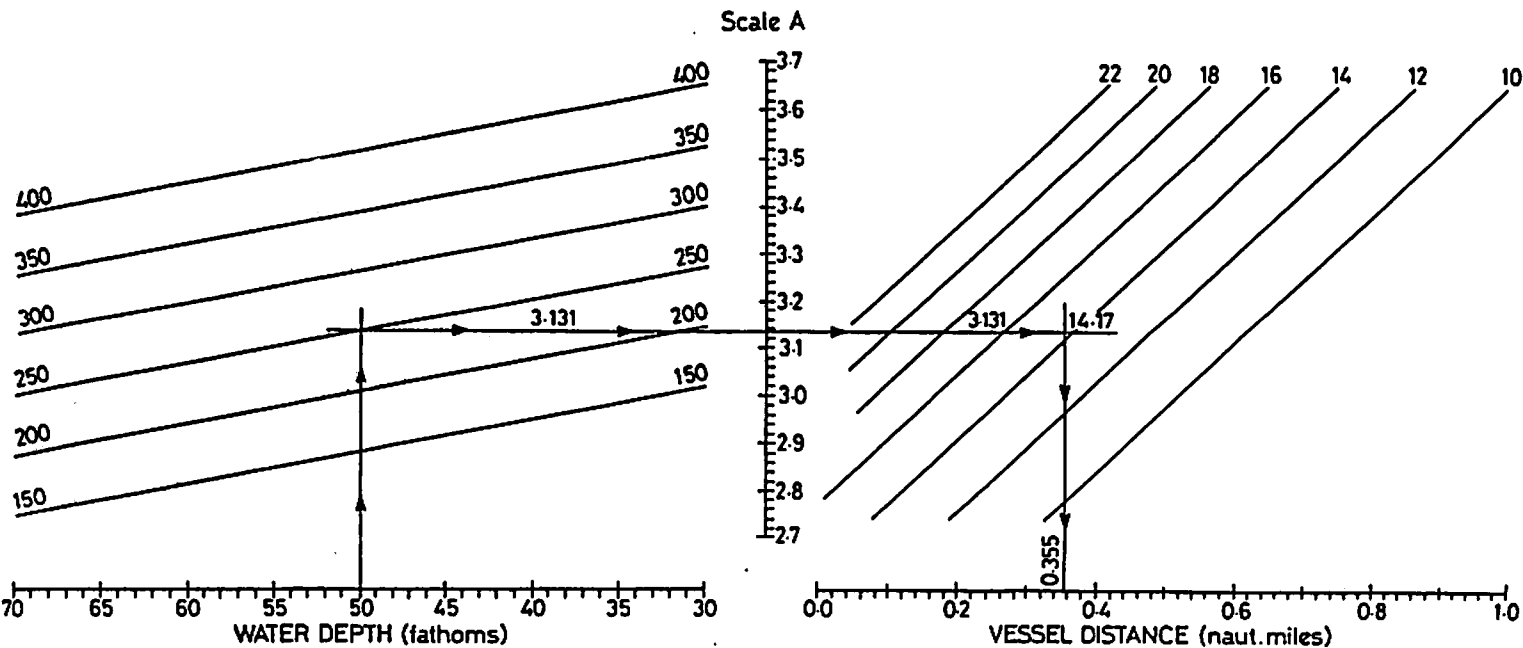
# HORIZONTAL OPENING

NET SPEED 3 knots



# VERTICAL OPENING

NET SPEED 3 knots



# HORIZONTAL OPENING (Wing End Spread)

